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IAEA SAFETY STANDARDS

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Evaluation of Seismic Safety for Nuclear

Installations

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FOREWORD

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1. INTRODUCTION

BACKGROUND

1.1. The present publication<u>This Safety Guide</u> provides guidance and procedures for<u>recommendations on</u> the evaluation of safety of nuclear installations against the effects generated by earthquakes.

1.2.1.1. This Safety Guide provides recommendations on meeting, in order to meet the applicable safety requirements statedestablished in the following safety standardspublications:

- IAEA Safety Standards Series No. GSR Part 4 (Rev. 1), Safety Assessment for Facilities and Activities [1];
- IAEA Safety Standards Series No. SSR-1, Site Evaluation for Nuclear Installations [2];
- IAEA Safety Standards Series No. SSR-2/1 (Rev. 1), Safety of Nuclear Power Plants: Design [3];
- IAEA Safety Standards Series No. SSR-2/2 (Rev. 1), Safety of Nuclear Power Plants: Operation [4];
- IAEA Safety Standards Series No. SSR-3, Safety of Research Reactors [5];
- IAEA Safety Standards Series No. SSR-4, Safety of Nuclear Fuel Cycle Facilities [6].

1.3.1.2. This Safety Guide addresses the requirements for both for existing and new nuclear installations. For an existing installation, safety assessments are required to be reviewed periodically and the review may —consider potential changes in site seismic hazard characterization [1] [2] [4] [5] [6].[1, 2, 4–6]. At the design stage of a new nuclear installation, it is required to be checked that the design provides for an adequate margin to protect items important to safety against levels of external hazards more severe than those selected for the design basis [3] [5] [6].[3, 5, 6]. In addition, it is required to be checked that the design of nuclear power plants provides for an adequate margin to protect items ultimately necessary to prevent an early radioactive release or a large radioactive release in the event of levels of natural hazards exceeding those considered for design [3]. Hence, the seismic safety assessments evaluations described in this Safety Guide can be performed either as part of the design development or as a process or a completelysubsequent and separate procedure from the design stage basis cases.

1.4.1.3. This Safety Guide is related to a number of other IAEA Safety Guides dealing with

seismic hazard and seismic design, including IAEA Safety Standards Series Nos SSG-9₇ (<u>Rev.1</u>), Seismic Hazards in Site Evaluation for Nuclear Installations [7], <u>NS-G-1.6SSG-67</u>, Seismic Design and <u>Qualification</u> for Nuclear <u>Power Plants [8], Installations</u> [9] and NS-G-3.6, Geotechnical Aspects of Site Evaluation and Foundations for Nuclear Power Plants [10]. In addition, Ref. [11] provides detailed information relevant to this Safety Guide.

<u>1.5.1.4.</u>Guidelines for the seismic safety evaluation of existing nuclear installations — <u>mainlyin</u> <u>particular</u> nuclear power plants — have been developed and used in many Member States since the beginning of the 1990s¹. More recently, <u>the</u> criteria and methods <u>appliedused</u> for <u>the</u> seismic safety evaluation of existing <u>nuclear</u> installations <u>have</u> started being used, <u>afterwith</u> some adaptation, <u>for assessingto assess</u> beyond design basis earthquake <u>conditionsevents</u> for new <u>nuclear installation</u> designs, prior to construction. This <u>assessmentevaluation of new designs</u> is different <u>thanfrom</u> the seismic design and qualification of the installation, which is <u>carfied</u> <u>outperformed</u> for the design basis earthquake following the guidelines in <u>NS-G-1.6 [8]SSG-67</u> [9]. The seismic safety evaluation of a new design is intended to explore beyond design basis <u>conditionsevents</u> for the new design².

1.6.1.5.Seismie The main difference between seismic safety evaluation differs from and seismic design and qualification [8]. The main difference is in the evaluation criteria used [9]. Design, as traditionally understood³, uses conservatively defined loads and capacities for structures, systems and components (SSCs) in order to meet the limits given in the design code. Thus, these methods are this design approach is aimed at meeting the limits given by the codes for the design level basis earthquake in every SSC. In this way, in order to demonstrate safety for the design level carthquake is demonstrated. On the other hand, in seismic safety evaluation, the aim is to establish the actual capacity capacities of the SSCs in the 'as-is'is condition and for use it in the evaluation of the seismic capacity of the nuclear installation as a whole. In doing this, The experience from exposure to past seismic events, testing, and analytical estimates of capacity are utilized in the seismic safety evaluation, and expert judgement plays a significant role. The 'as-is'is condition of the nuclear installation includes the 'its as-built',

¹ The development and use of guidelines on the seismic safety evaluation of existing nuclear installations started in the United States of America, where the application of such guidelines were developed and their application to all existing nuclear power plants was required by national regulations. ² Some Member States used these methodologies as a complementary technical support and they should not be solely

⁻Some Member States used these methodologies as a complementary technical support and they should not be solely used to comply with Requirements 17 of SSR 2/1 or equivalent requirements from SSR 3 or SSR 4 ³ The final seismic safety evaluation to check that the design provides for an adequate margin to protect items important

<u>"built, as-operated', operated, as-modified'modified</u> and <u>as-maintained'maintained</u> conditions<u>of</u> the installation, and its condition of ageing at the time of the <u>assessmentevaluation</u>.

<u>1.7.1.6.</u>The terms used in this Safety Guide, <u>including the definition of a graded approach</u>, are to be understood as defined in the IAEA Safety Glossary [12]. Explanations of terms specific to this Safety Guide are provided in footnotes.

<u>1.8.1.7.</u> The present publication supersedes the <u>This</u> Safety Guide on <u>supersedes IAEA Safety</u> <u>Standards Series No. NS-G-2.13</u>, Evaluation of Seismic Safety for Existing Nuclear Installations⁴.

OBJECTIVE

1.9.1.8. This The objective of this Safety Guide provides to provide recommendations and guidance in relation toon the seismic safety evaluation of nuclear installations, meeting in order to meet the applicable safety requirements from Refs. established in GSR Part 4 [1], SSR-1 [2], SSR-2/1 (Rev. 1) [3], SSR-2/2 (Rev. 1) [4], SSR-3 [5] and SSR-4 [6]. For existing installations, such an evaluation may be prompted by a seismic hazard perceived to be greater than that originally established in the design basis, by new regulatory requirements, by new findings on the seismic vulnerability of SSCs, or by the need to demonstrate performance for beyond design basis earthquake conditions of nuclear installations, the seismic safety evaluation is motivated by the need to demonstrate that the safety margins above the design basis earthquake are sufficient to avoid cliff edge effects⁵ and, in the case of nuclear power plants, sufficient to protect items ultimately necessary to prevent radioactive releases in the event of an earthquake with a severity exceeding the onethat considered for design.

<u>1.10,1.9.</u> This Safety Guide is intended for use by regulatory bodies responsible for establishing regulatory requirements, by designers and safety analysts involved in the <u>seismic</u> design of new nuclear installations and by operating organizations of existing installations directly responsible

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⁴ INTERNATIONAL ATOMIC ENERGY AGENCY, Evaluation of Seismic Safety for Existing Nuclear Installations, IAEA Safety Standards Series No. NS-G-2.13, IAEA, Vienna (2009).

⁵ A 'cliff edge effect', in a nuclear power plant, is an instance of severely abnormal plant behaviour caused by an abrupt transition from one plant status to another following a small deviation in a plant parameter, and thus a sudden large variation in plant conditions in response to a small variation in an input [3]-. In the context of seismic safety, the term 'plant parameter' in this definition refers to seismic ground motion at the plant site.

for the execution of the conducting seismic safety evaluation evaluations and upgrading seismic safety programmes, as applicable.

SCOPE

<u>1.10.</u> This Safety Guide addresses an extended rangeall types of new and existing nuclear installations, that is: land based stationary nuclear as defined in the IAEA Safety Glossary [11], as follows:

- (a) Nuclear power plants, research;
- (b) Research reactors (including subcritical and critical assemblies) and any adjoining radioisotope production facilities;-storage
- (c) Storage facilities for spent fuel; facilities
- (d) Facilities for the enrichment of uranium; nuclear
- (e) Nuclear fuel fabrication facilities; conversion
- (f) Conversion facilities; facilities
- (g) Facilities for the reprocessing of spent fuel; facilities
- (h) Facilities for the predisposal management of radioactive waste arising from nuclear fuel cycle facilities; and nuclear
- (i) Nuclear fuel cycle related research and development facilities [11].

Most of the recommendations_provided in this Safety Guide are independent of the type of nuclear installation or the reactor type, but aspects such as performance criteria and systems modelling are specific to each installation type. The recommendations for nuclear power plants are also applicable to other nuclear installations through the use of a graded approach.

1.11. For the <u>purposespurpose</u> of this Safety Guide, <u>sexisting</u><u>existing</u> nuclear installations are those installations that are either (a) at the operational stage (including long term operation and extended temporary shutdown periods)⁶; or (b) at a <u>preoperational pre-operational</u> stage for which the construction of structures, <u>the</u> manufacturing, installation and/or assembly of components and systems, and commissioning activities are significantly advanced or fully completed. In existing nuclear installations that are at the operational and pre-operational stages, a change of the original design bases, such as for (e.g. a new seismic hazard at the site₇) or a change in the regulatory requirements regarding the consideration of seismic hazard and/or seismic design of the installation, <u>maynight</u> lead to important <u>physicaltechnical</u> modifications.

⁶ The operational stage ends with the permanent removal of all radioactive material. 12

1.12. For the purpose of this Safety Guide, <u>"new2new</u> nuclear installations are those installations for which thewhose design has reached a level of development inat which a detailed definition of SSCs is available, including the data <u>itemizedlisted</u> in paras 4.2—_4.5. Typically, a <u>"new" nuclear installation</u>⁷, asAs understood in this Safety Guide, <u>is-new nuclear</u> <u>installations are not yet</u> constructed, or construction is at a very early stage.⁸

1.13. Three <u>assessment</u> methodologies are <u>discussedaddressed</u> in detail in this Safety Guide: the deterministic approach, generally represented by <u>Seismic Margin Assessmentseismic</u> <u>margin assessment</u> (SMA), the <u>Seismic Probabilistic Safety Assessmentseismic probabilistic</u> <u>safety assessment</u> (SPSA), and a combination of SMA and SPSA known as '<u>probabilistic safety</u> <u>assessment (PSA-)</u> based <u>Seismic Margin Assessment'.SMA'</u>. Variations of these approaches or alternative approaches may <u>also</u> be demonstrated to be acceptable <u>also</u>, as <u>discussed in(see</u> Section 3-).

STRUCTURE

1.14. Section 2 itemizes identifies the safety requirements addressed by this Safety Guide, and describes general concepts and provides general concepts and general recommendations omrelating to the seismic safety evaluation of nuclear installations. Section 3 provides recommendations on the selection of the methodology for performing the seismic safety assessmentevaluation. Section 4 provides recommendations on datathe requirements (for data collection and investigations), both for new and for existing installations. Section 5 isforms the core of this Safety Guide. It provides; it focuses on nuclear power plants, providing recommendations on considerations in relation to the assessment of seismic hazards-and with, the seismic capability necessary for level 4 of the defence-in-depth level 4, then provides recommendations on the concept, and the implementation of the SMA, PSA-based SMA and SPSA methodologies for seismic safety evaluation focused on nuclear power plants. Section 6 provides specific recommendations on applying a graded approach to the seismic safety evaluation of nuclear installations other than nuclear power plants (with reference to Section 5 where appropriate). Section 7 presentsprovides recommendations on the use of seismic safety evaluation results, including for potential seismic upgrading. Section 8 provides recommendations on the management system to be put in placeestablished for the performance

²-New installations may include a standard design based on generic site parameters, for which the site has not been specified <u>8</u> A new nuclear installation may also be a standard design based on generic site parameters, for which the site has not yet been specified.



of all <u>seismic safety evaluation</u> activities, and <u>it</u> identifies the need for configuration management in future activities to maintain the seismic capacity as evaluated. Sections 1-4, 7, and <u>6-8</u> apply (in total<u>full</u> or in part) to all nuclear installations. Section 5 is focused on nuclear power plants <u>but can be applied to other nuclear installations through the use of a graded approach as described in Section 6.</u>

1.15. The appendix to this Safety Guide presents seismic failure mode considerations for different types of SSCs. The annex provides an example of criteria for defining seismic design classes and performance targets in a nuclear installation.

2. GENERAL CONSIDERATIONS FOR EVALUATION OF SEISMIC SAFETY FOR NUCLEAR INSTALLATIONS

SAFETY REQUIREMENTS FOR APPLICABLE TO SEISMIC SAFETY EVALUATION

Safety assessment

2.1. <u>As-Various safety requirements</u> established in the GSR Part 4 (Rev. 1) [1], the following requirements should be applied for apply to seismic design robustness and periodic review of seismic safety:

2.2.2.1.. Requirement 10 of GSR Part 4 (Rev. 1) [1] states:

"It shall be determined in the safety assessment whether a facility or activity uses, to the extent practicable, structures, systems and components of robust and proven design."

Requirement 13 of GSR Part 4 (Rev. 1) [1] states that "It shall be determined in the assessment of defence in depth whether adequate provisions have been made at each of the levels of defence in depth."

Paragraph 4.48A of GSR Part 4 (Rev. 1) [1] states that <u>(footnote omitted)</u> "Where practicable, the safety assessment shall confirm that there are adequate margins to avoid cliff edge effects that would have unacceptable consequences."

Requirement 15 of GSR Part 4 (Rev. 1) [1] states that "**Both deterministic and probabilistic** approaches shall be included in the safety analysis."

Requirement 24 of GSR Part 4 (Rev. 1) [1] states that: "The safety assessment shall be periodically reviewed and updated."

2.3.2.2.Similar provisions shouldare required to be applied to research reactors and to nuclear fuel cycle facilities, as established in Requirement 5 of SSR-3 [5], and Requirement 5 of SSR-4 [6], respectively.

Hazard assessment

2.4. As established in SSR 1 [2], the following requirement should be applied to address With regard to potential changes in the perceived seismic hazard:

2.5.2.3., Requirement 29 of SSR-1 [2] states:

"All natural and human induced external hazards and site conditions shall be periodically reviewed by the operating organization as part of the periodic safety

review and as appropriate throughout the lifetime of the nuclear installation, with due account taken of operating experience and new safety related information."

Design

As Margin provided by the design

2.6. <u>Various safety requirements</u> established in SSR-2/1 (Rev. 1) [3], the following requirements should be applied regarding apply to the seismic margin to be provided by the design of nuclear power plants⁹:

2.7.2.4.. Requirement 17 of SSR-2/1 (Rev. 1) [3] states:

"All foreseeable internal hazards and external hazards, including the potential for human induced events directly or indirectly to affect the safety of the nuclear power plant, shall be identified and their effects shall be evaluated. Hazards shall be considered in designing the layout of the plant and in determining the postulated initiating events and generated loadings for use in the design of relevant items important to safety for the plant."

• • •

Paragraph 5.21 of SSR-2/1 (Rev. 1) [3] states: (footnote omitted):

"The design of the plant shall provide for an adequate margin to protect items important to safety against levels of external hazards to be considered for design, derived from the hazard evaluation for the site, and to avoid cliff edge effects."

Paragraph 5.21A of SSR-2/1 (Rev. 1) [3] states:

"The design of the plant shall also provide for an adequate margin to protect items ultimately necessary to prevent an early radioactive release or a large radioactive release in the event of levels of natural hazards exceeding those considered for design, derived from the <u>hazardshazard</u> evaluation for the site."

2.8.2.5.Similar provisions shouldare required to be applied to research reactors and to nuclear

⁹ Paragraph 1.3 of SSR-2/1 (Rev. 1) [3] <u>states-acknowledges</u> that "<u>it</u>] might not be practicable to apply all the requirements of this Safety Requirements publication to nuclear power plants that are already in operation or under construction"," Hence, for the purposes of the present Safety Guide, the requirements <u>quoted</u> here <u>may beare</u> considered applicable only to new nuclear power plants.



fuel cycle facilities, as established in Requirement 19of<u>19</u> of SSR-3 [5], and Requirement 16 of SSR-4 [6], respectively.

Operation

As Considering effects of changes during operation

2.9. <u>Various safety requirements</u> established in SSR-2/2 (Rev. 1) [4], the following requirements should be applied during operation of nuclear power plants apply to assessassessing the consequences of changes in the perceived seismic hazard;

2.10.2.6. during operation of nuclear power plants. Requirement 12 of SSR-2/2 (Rev. 1) [4] states:

"Systematic safety assessments of the plant, in accordance with the regulatory requirements, shall be performed by the operating organization throughout the plant's operating lifetime, with due account taken of operating experience and significant new safety related information from all relevant sources."

Paragraph 4.44 of SSR-2/2 (Rev. 1) [4] states:

"Safety reviews such as periodic safety reviews or safety assessments under alternative arrangements shall be carried out throughout the lifetime of the plant, at regular intervals and as frequently as necessary (typically no less frequently than once in ten years). Safety reviews shall address, in an appropriate manner: the consequences of the cumulative effects of plant ageing and plant modification; equipment requalification; operating experience, including national and international operating experience; current national and international standards; technical developments; organizational and management issues; and site related aspects. Safety reviews shall be aimed at ensuring a high level of safety throughout the operating lifetime of the plant."

GENERAL CONCEPTS FOR EVALUATION OF-SEISMIC SAFETY FOR<u>EVALUATION</u> <u>OF</u> NUCLEAR INSTALLATIONS

2.11.2.7. Well designed and <u>well</u> maintained nuclear installations, especially nuclear power plants, have an inherent capability to resist <u>beyond design basis</u> earthquakes-<u>larger than the</u> earthquake considered in their design. This inherent capability or robustness — usually described in terms of the <u>seismic margin margin</u> — is a direct consequence of (ia) the conservatism that is present in the seismic design and qualification procedures used according to previous or current practices in earthquake engineering; and (iib) the fact that in the design

of nuclear power plants the seismic loads may not be the governing loads for some SSCs.¹⁰-

2.12.2.8. Typically; The current criteria for seismic design and qualification applicable to nuclear power plants <u>often</u> introduce <u>substantial</u> seismic design margins, <u>often</u> <u>substantial</u>, <u>which_that are not fully quantified by</u> the traditional design process <u>does not by itself quantify</u> in its <u>entirety</u>. The process by which <u>seismic</u> margins develop through the various stages of the analysis, design and construction <u>maymight</u> lead to large variations in the margins throughout the nuclear installation. The seismic margin typically varies from one location in the installation to another, from one SSC to another, and from one <u>location to another inpart of</u> the same structure to <u>another</u>.¹¹- Consequently, when evaluating the seismic safety of a nuclear installation, there should be a detailed examination of the actual design methods and, for existing installations, of the <u>fas-is²is</u> condition, in order to understand the sources of seismic capacity all over the nuclear installation since this may lead to complacency in the seismic safety evaluation.

2.13.2.9. The methodologies presented in this Safety Guide are intended for evaluating and quantifying the seismic margin over the design basis earthquake offor a particular <u>nuclear</u> installation. The Through understanding the realistic seismic response of the SSCs, in terms of their safety function, should be understood. From this understanding, functions, the maximum seismic eapacity of the SSCs demand for which there is high confidence that the safety functions are will be fulfilled, can be derived. High confidence determined. The SSC capacities of the SSCs are high confidence derived in this way can be used to assess the seismic safety margin of the installation as a whole.

2.14.2.10. The seismic safety evaluation of an existing <u>nuclear</u> installation strongly depends on the actual condition of the installation at the time the <u>assessmentevaluation</u> is performed. This key condition is denoted the <u>sas-is is</u> condition, indicating that an earthquake, when it occurs, <u>affects will affect</u> the installation in its <u>actualcurrent</u> condition, and <u>that</u> the response and

¹⁰ The existence of <u>seismic</u> margins has been demonstrated not only through the implementation of SMA orand SPSA methodologies for existing nuclear power plants in several Member States, but also by the performance of <u>some</u> plants in large earthquakes. Those plants<u>that</u> have experienced large earthquakes, which exceeded their <u>beyond</u> design basis, <u>earthquakes</u> and <u>have survived the earthquakesproved their integrity</u> with little or no damage.

¹¹ One of the main reasons for this variation, as mentioned in para. 2.7, is the fact that nuclear installations are designed for a wide range of internal and external extreme loads, for example, pressure and other environmental loads due to accident conditions, an aircraft crash, a tornado or a pipe break. Therefore, as mentioned in para. 2.7, seismic loads may not be the governing loads for some SSCs. Another reason is the method of equipment qualification, in which envelope-type response spectra are generally used.

capacity of the installation will depend on its <u>actualcurrent</u> physical and operating configuration. The <u>sas-is2is</u> condition <u>is</u> typically <u>consistsestablished on the basis</u> of the original design, <u>taking into account</u> design changes during construction and operation, <u>unintended</u> <u>deviations from the design</u>, and ageing. That is why the upkeep of up-to-date, as-built design documentation and <u>of-documentation from the</u> ageing management programme is very important. The <u>sas-is2is</u> condition of the installation should <u>beprovide</u> the baseline for any seismic safety evaluation.

2.15.2.11. Seismic safety evaluationevaluations performed on the basis of the as-is condition of the <u>nuclear</u> installation, should <u>emphasizebe</u> pragmatic <u>evaluations</u> rather than using extensive complex analyses. Non-linear analyses of relatively simple structural models or the use of higher damping values and ductility factors — provided that they are <u>used with caretechnically</u> justified and are consistent with allowable deformations <u>considering the as-is condition of the installation</u> — may, <u>however</u>, be particularly helpful in understanding post-elastic behaviour. Numerous field observations and research and development programmes have demonstrated a high seismic capacity results when the ductile behaviour of SSCs is able to accommodate large strains.

2.16.2.12. When a reliable seismic hazard analysis is available for a particular site (see SSG-9 (Rev.1) [7]), seismic safety evaluation should use a realistic definition of the hazard dominant earthquake motion for the selected annual frequency of exceedance, (in terms of amplitude, duration, directivity and frequency content.) for the selected annual frequency of exceedance should be used for the seismic safety evaluation. When there are several dominant seismic sources that lead to very different motion characteristics (e.g., far field and, near field), the feasibility of using several motion characterizations and, therefore, assessing seismic safety (including safety margins) against each of them, should be considered.

REASONS TO PERFORM SEISMIC SAFETY EVALUATIONS

New nuclear installations

2.17.2.13. In accordance with the requirements established in GSR Part 4 [1], SSR-2/1 (Rev. 1) [3], SSR-3 [5], and SSR-4 [6] (see paras. 2.1, 2.2, 2.4 and 2.52.1–2.5 of this Safety Guide), an evaluation of the seismic safety of new nuclear installations is required to be performed as a part of the safety assessment, when the design is completed, to verify that the safety margins above the design basis earthquake are sufficient to avoid cliff edge effects. In addition, in the case of a nuclear power plant, the seismic safety evaluation is required to verify that the margins are

sufficient to protect items ultimately necessary to prevent radioactive releases in the event of an earthquake with a severity exceeding <u>the onethat</u> considered for design-(see SSR-2/1 (Rev. 1) [3]). This safety assessmentevaluation should be reflected in the <u>safety analysis report for</u> the installation (see Safety Standards Series No. SSG-61, Format and Content of the Safety Analysis Report of the installation for Nuclear Power Plants [13]-). Recommendations on the level of seismic margin to be achieved in a new <u>nuclear</u> installation are provided in <u>SSG-67</u> IAEA Safety Standards Series No. DS490, Seismic Design of Nuclear Installations [9].

2.18.2.14. In connection with para 2.13, the The design of a new nuclear power plant needs is required to meet two requirements provide for: (a) Adequate an adequate seismic margin forto protect items important to safety to provide protection against seismic hazardshazard levels exceeding those considered for design and to avoid cliff edge effects (see para. 5.21 of SSR-2/1 (Rev. 1) [3]); and (b) Adequate an adequate seismic margin to protect items ultimately necessary to prevent an early radioactive release or a large radioactive release in the event of levels of natural hazards exceeding those considered for design (see para. 5.21A of SSR-2/1 (Rev. 1) [3]). The seismic margin needed to meet (b) normally applies to a reduced set of SSCs and normally showsgenerally results in larger plant state margins- than the seismic margin needed to meet (a).

Existing nuclear installations

2.19.2.15. In accordance with the requirements established in GSR Part 4 (Rev. 1) [1], SSR-1 [2], SSR-2/2 (Rev. 1) [4], SSR-3 [5] and SSR-4 [6] (see paras: 2.1, 2.3, 2.1-2.3 and 2.62.6 of this Safety Guide), and in line with international practice, an evaluation of the seismic safety of an existing nuclear installation is required to be performed in the event of any one of the following cases:

- (a) Evidence of a significant increase in the seismic hazard at the site, arising from new or additional data (e.g. newly discovered seismogenic structures, newly installed seismological networks or new paleo-seismological evidence), new methods of seismic hazard assessment, and/or the occurrence of actual earthquakes that affect the installation;
- (b) Regulatory requirements, such as <u>thea</u> requirement for periodic safety reviews, that take into account the <u>state</u> of <u>knowledge</u> and the actual condition of the installation;
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- Inadequate seismic design, generally due to the <u>vintagevery old design</u> of the <u>facilityinstallation;</u>
- (d) New technical findings, such as vulnerability of selected structures and/or non-structural elements (e.g. masonry walls), and/or of systems or components (e.g. relays);
- New experience from the occurrence of actual earthquakes (e.g. better recorded ground motion data-and-the, observed performance of SSCs);
- (f) The need to address the performance of the installation for beyond design basis earthquake ground motions in order to provide confidence that there is no <u>cliff</u> edge <u>effect'effect</u>, that is, to demonstrate that no significant failures would occur in the installation if an earthquake were to occur that was somewhat <u>greaterstronger</u> than the design basis earthquake;
- (g) A programme for<u>of</u> long-term operation, <u>extending that extends</u> the <u>lifelifetime</u> of the plant, for which such an evaluation is required if applicable.

2.20.2.16. If, for the reasons listed in para. 2.15 or for other reasons, a seismic safety evaluation of an existing nuclear installation is required, the purposes of the evaluation should be clearly established before the evaluation process is initiated. This is because there are significant differences among the available evaluation procedures methodologies and acceptance criteria, depending on the purpose of the evaluation $\frac{12}{2}$ (see Section 3). In this regard, the objectives of the seismic safety evaluation may include one or more of the following:

- (a) To demonstrate the seismic safety margin beyond the original design basis earthquake and to confirm that there are no cliff edge effects.
- (b) To identify weak links in the installation and its operations with respect to seismic events.
- (c) To evaluate a group of installations (e.g. all the installations in a region or a State); in order to determine their relative seismic capacity and/or their risk ranking. For this purpose, similar and comparable methodologies should be adopted.
- (d) To provide input for integrated risk informed decision-_making.
- (e) To identify and prioritize possible upgrades.

¹² Available evaluation procedures, and the differences between them, are presented and discussed in Section 3. 21

- (f) To assess risk metrics (e.g. core <u>and/or fuel</u> damage frequency<u>-and</u>, <u>early radioactive</u> release frequency or large <u>earlyradioactive</u> release frequency) against regulatory requirements, if any.
- (g) To assess installation capacity metrics (e.g. <u>systems-system</u> level and installation-level fragilities or, <u>'high confidence of low probability of failure' (HCLPF) capacity</u>¹³ capacities) against regulatory expectations.

2.21.2.17. The objectives of the seismic safety evaluation of an existing <u>nuclear</u> installation should be established in line with the regulatory requirements, and in consultation and agreement with the regulatory body. Consequently, and in accordance with such objectives, the level of seismic input motion, the methodology for capacity assessment and the acceptance criteria to be applied, including the <u>requirednecessary</u> end products, should be defined. In particular, for evaluating seismic safety for seismic events more severe than the event specified in the <u>original event of an earthquake with a severity exceeding that considered for</u> design-basis, the safety objectives should include the functions-<u>required</u> to be ensured and the failure modes to be prevented during or after the earthquake's occurrence.

2.22.2.18. The final documentation to be produced at the end of the <u>seismic safety</u> evaluation of an existing <u>nuclear</u> installation should be identified <u>fromat</u> the <u>startoutset</u>, in agreement with the regulatory body, and should be consistent with the established purpose of the evaluation programme (see paragraph 8.6). The end <u>productsproduct(s)</u> of <u>these evaluations the evaluation</u> may be one or more of the following:

- Metrics of the seismic capacity of the nuclear installation in deterministic and/or probabilistic terms;
- (b) Quantification of the seismic risk;
- Identification of SSCs with low seismic capacity, and the associated consequences for <u>plantinstallation</u> safety, to be used for use in decision-_making foron seismic upgrade programmes;
- (d) Identification of operational modifications to improve seismic capacity;

¹³ The High Confidence Low Probability of Failure (HCLPF) capacity is the earthquake motion level at which there is a high confidence of a low probability of failure. <u>of SSCs. The</u> HCLPF capacity is a measure of seismic margin (see Sectionparas 5.44–5.47).



- (e) Identification of improvements to housekeeping practices (e.g. storage of maintenance equipment);
- (f) Identification of interactions with equipment and piping, including fire protection systems, high enthalpy lines and utilities;
- (g) Identification of actions to be taken before, during, and after the occurrence of an earthquake that affects the installation, including arrangements for operational and management response, analysis of the obtained instrumental seismic records obtained and performed inspections performed, and the integrity evaluations to be performed as a consequence;
- (h) A framework to provide input to risk informed decision-making-
- (i) A framework for the revision of the seismic categorization of SSCs.

CONSIDERATION OF RELEVANT ASPECTS RELATED TO SEISMIC HAZARD

2.23.2.19. An initial step of any seismic safety evaluation — in parallel with the collection of relatedrelevant data as indicated in Section 4 — should be to identify the seismic hazards with regard toon the basis of which the seismic safety of the installation will be evaluated. In this respect, the seismic hazards specific to the site should be assessed in relation to three main elements¹⁴:

- (a) Evaluation of the geological stability of the site [7] [10], with two main objectives pertaining to non-vibratory ground motions:
 - (i) To verify the absence of any capable fault that could produce <u>significant</u> differential ground displacement phenomena underneath or in the close vicinity of buildings and structures important to safety. If there exists evidence that indicates the possibility of a capable fault in the site area or site vicinity, the fault displacement hazard should first be assessed in accordance with the guidance provided in SSG-9 (Rev.1) [7].
 - (ii) To characterize potential permanent ground deformation phenomena (i.e.g. liquefaction, slope instability, excessive settlement, subsidence or, collapse).

¹⁴ In most cases, it is foreseen that a seismic <u>hazardshazard</u> assessment will be available as part of the site investigation or a periodic revaluation of the hazards. The available hazard assessments will need to be reviewed to determine if they are adequate for the purposes of the seismic safety evaluation being performed.

- (b) Characterization of the severity of the seismic ground motion at the site, that is, assessment of the vibratory ground motion parameters, taking into consideration the full scope of the seismotectonic effects at the four <u>spatial</u> scales of investigation¹⁵ and as recommended in SSG-9 (Rev.1) [7].
- (c) Evaluation of other concomitant phenomena such as earthquake induced river flooding due to dam-seismically induced failure of dams or water retaining structures, coastal flooding due to tsunami, and landslidesseismically induced slope instabilities.

2.24.2.20. In general, the seismic hazard assessment may be performed using a deterministic or a probabilistic approach, depending on the objectives and requirements of the seismic safety assessmentevaluation. In either case, both the aleatory and the epistemic uncertainties should be taken into consideration.

2.25.2.21. The evaluations recommended in paras. 2.19 (a) and 2.19 (c) of this Safety Guide should be performed in all cases for a seismic safety evaluation evaluations, regardless of the methodology used and in accordance with SSG-9 (Rev.1) [7], NS-G-3.6 [10] and IAEA Safety Standards Series No. SSG-18, Meteorological and Hydrological Hazards in Site Evaluation for Nuclear Installations [14]. For evaluating the geotechnical hazards (e.g. liquefaction, slope instability, subsidence, collapse), the most <u>currentrecent</u> available seismic hazard parameters should be used.

2.26.2.22. With respect to para. 2.19 (b) of this Safety Guide,(b), the recommendations on assessing the seismic hazard at the site are dependent on the objectives of the <u>seismic safety</u> evaluation. A site-specific ground motion seismic hazard assessment is generally preferred, and <u>isshould be considered</u> a prerequisite that should, to be carried out,implemented as recommended in SSG-9 (Rev.1) [7], when the objectives of the evaluation include the assessment of the seismic risk posed by the installation or <u>the assessment of risk-based</u> metrics for the SSCs. On the other hand, <u>ita site specific ground motion seismic hazard assessment</u> should not be considered a prerequisite when the objective of the evaluation is to determine the seismic margin above a predefined reference level earthquake and/or to rank the SSCs contributing to the installation-level seismic capacity to withstand that reference level earthquake for identification of seismic weak links. However, even in those cases with these

¹⁵ In SSR-1 [2] and SSG-9 (Rev.1) [7], four <u>spatial geographical scales</u> of <u>geological</u>, <u>geophysical and geotechnical</u> investigations are defined: (1) <u>regional' regional (radius Rtypically</u> about 300 km-); (2) <u>hear region², R-noregional (radius typically not</u> less than 25 km-); (3) <u>site vieinity', R-novicinity (radius typically not</u> less than 5 km-); and (4) site area, <u>R (radius typically</u> about 1 km-).

<u>objectives</u>, a seismic hazard assessment should <u>still</u> be performed when site-_specific information indicates that the ground motion characteristics (e.g. spectral shape) might differ significantly from the ones assumed for design.

2.27.2.23. A site-_specific probabilistic seismic hazard assessment [7]-should be performed when the objectives of the seismic safety assessmentevaluation entail the following:

- (a) Calculation of risk metrics (e.g. core <u>and/or fuel</u> damage frequency<u>and large</u> early release frequency;
- (b) Establishment of a risk management tool for risk informed decision_making;
- (c) Determination of the relative risk between seismic and other internal and external hazards;
- (d) Provision of a tool for cost-benefit analysis tool for decision-making in relation to plant upgrades.

2.28.2.24. For the SMA and PSA-based SMA methodologies, the reference level earthquake¹⁶ defines the seismic input that should be used in the seismic safety evaluation. The reference level earthquake (see also para. 5.5) should not be understood interpreted as a new design basis earthquake (see also para. 5.5). It should be understood, but rather as a tool to determine the seismic margin and seismic weak links¹⁷ of the installation and its seismic 'weak links¹⁴⁸. The reference level earthquake should be sufficiently larger than the design basis earthquake, to ensure the extent that it challenges the seismic capacity of the SSCs so that an installation-level HCLPF can be determined and the 'any weak links' (if any)links can be identified. The reference level earthquake is typically specified by means of a spectral shape, anchored at a peak ground acceleration level, defining the seismic motion at a given control point. The seismic input for a seismic safety evaluation should not be less than a peak ground acceleration of 0.1 g at the free field or foundation level.

¹⁴ In this context, a seismic 'weak link' is a non-redundant SSC or identical redundant SSCs (affected by common cause failure) which has a smaller capacity than the majority of the other SSCs and, as such, it could be controlling the installation level seismic capacity.



¹⁶ In the literature on SMA methodology, this <u>a</u> reference level <u>earthquake</u> is sometimes <u>knownreferred to</u> as the<u>a</u> 'review level earthquake' or the 'seismic margin earthquake'.
<u>17</u> In this context, 'seismic weak links' are non-redundant SSCs or identical redundant SSCs (affected by common cause)

¹² In this context, 'seismic weak links' are non-redundant SSCs or identical redundant SSCs (affected by common cause failure) which have a smaller capacity than the majority of the other SSCs, and, as such, could govern the installation level seismic capacity.
⁴⁴ In this context, a seismic 'weak link' is a non-redundant SSC or identical redundant SSCs (affected by common cause)

2.29.2.25. For the SPSA methodology, the reference level earthquake¹⁹ is defined using the site-_specific probabilistic seismic hazard assessment results. Generally, thosethese results include seismic hazard curves defining the annual frequency of exceedance (often referred to as the 'annual probability of exceedanceexceedance') of ground motion parameters (e.g. spectral accelerations), associated response spectra (e.g. uniform hazard spectra) and characteristics of the dominant source parameters (e.g. magnitude and distance from the site). The reference level earthquake should be defined at an annual frequency of exceedance that corresponds to an earthquake severity that significantly contributes to the seismic risk of the nuclear installation. When there are several dominant seismic sources which that lead to very different motion characteristics (e.g. far field and, near field), the overall seismic hazard curves may be split into multiple, mutually exclusive; contributions, and multiple corresponding reference level earthquakes may be defined for the seismic safety assessment evaluation. In that this case, the seismic risk computed for each contribution should be added upcombined to obtain the total risk.

EVALUATION OF SEISMIC SAFETY FOR <u>MULTI FACILITY SITES WITH MULTIPLE</u> NUCLEAR INSTALLATIONS

2.30.2.26. For sites with multiple nuclear installations (mainlygenerally nuclear power plants) and/or with nuclear power plants that credit forhave a significant number of shared systems and resources, seismic safety evaluation is required to consider or impact of accident phenomena between multiple nuclear installations, potential interactions between the installations. Safety should be considered in the seismic safety evaluation. The evaluation of multi-facility-sites provides will provide risk insights thatto help minimize the risk of multi-facility-sites accidents in several installations (e.g. due to shared systems and resources) and to-maximize the benefits associated towith shared systems and resources among units. The Multiunit-installations. Multi-unit_PSA is an appropriate methodology for considering potential interactions in a multiunitmulti-unit context. TheRecommendations on this methodology are provided in IAEA Safety Standards Series No. DS523, Development and Application of Level 1 Probabilistic Safety Assessment for Nuclear Power Plants [14] and IAEA Safety Standards Series No. DS524, Radiation Protection Aspects of Design for Nuclear Power Plants [15]; the

¹⁹ The <u>'In this context, the</u> reference level <u>earthquake' concept, as used in the present Safety Guide (see para.</u> 5.5),<u>earthquake</u> is not to be confused with the seismic level <u>that is usedthreshold</u> sometimes <u>used</u> in SPSA as a threshold for <u>the</u> explicit calculation of fragilities, (when <u>the level is below</u>, the threshold), and for <u>the</u> assignment of generic fragilities, (when <u>the level is above</u>, the threshold).

technical background of the methodology can be found is explained in Refs. [15], [16], [17] and [18]. [16, 17].

CONSIDERATION OF SEISMIC SAFETY EVALUATION AT THE DESIGN STAGE

2.31.2.27. At the design stage for new nuclear installations, SPSA or PSA-based SMA methodologies are typically used to addressmeet the requirements described indicated in paras. 2.13 and 2.14 of this Safety Guide. At the design stage,²⁰ The assessment methodologies are limited toby the information available inup to the design phases and cannot rely on anstage; the as-built and as-operated installation. All tasks are similar with the one used-information cannot be utilized in the same way that it is for existing nuclear installations and the differences consists only in the availability of information. Instead of as built and as operated information, at the design stage, methodologies should rely on $_{s}$ as designed information only. Seismicand operational experience feedback from similar designs should be used in applying these methodologies at the design stage. Moreover, physical seismic evaluation walkdowns cannot be conducted at the design this stage.

2.32.2.28. During development of the design, seismic safety evaluation should be used to address and eliminate seismic vulnerabilities identified in the past, to check the effectiveness of the defence in depth provisions, to provide insights for setting performance targets consistent with the seismic safety goals, and to optimize the robustness of seismic design.

CONSIDERATION OF SEISMIC SAFETY EVALUATION AT THE LICENSING STAGE

2.33.2.29. At the licensing stage, the detailed-design is completed, and the_site-_specific seismieseismically induced hazards are known. For nuclear power plants, SPSA methodology is typically used to provide input tofor the final safety analysis (for recommendations on the reporting of probabilistic safety assessment in the safety analysis report-(, see Section 3.15 of SSG-61 [13]). The seismic safety evaluation should provide assurance that the seismic design is adequate for the site-specific seismic conditions. ParticularlyIn particular, the SPSA for new nuclear installations provides risk insights, in conjunction with the assumptions made, and contributes to identifyidentifying and supportsupporting requirements importantrelated to the seismic design of the plant.

2.34.2.30. After the plant is builthas been constructed and operation starts, the seismic safety

²⁰ Some Member States use these methodologies as complementary technical support; they are not intended to be used alone to meet the relevant requirements of SSR-2/1 (Rev. 1) [3], SSR-3 [5] or SSR-4 [6].

evaluation performed <u>atbefore</u> the <u>licensing stageoperating licence was granted</u> should be updated to reflect <u>the</u> as-built and as-operated conditions.

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3. SELECTION OF THE<u>METHODOLOGY FOR EVALUATION OF</u> SEISMIC SAFETY ASSESSMENT METHODOLOGY

3.1. In accordance with Requirement 15 of GSR Part 4 (Rev. 1) [1], both deterministic and probabilistic approaches are required to be included in the safety analysis. Paragraph 4.53 of GSR Part 4 (Rev. 1) [1] states:

"Deterministic and probabilistic approaches have been shown to complement one another and can be used together to provide input into an integrated decision making process. The extent of the deterministic and probabilistic analyses carried out for a facility or activity shall be consistent with the graded approach."

3.1.3.2. The selection of the seismic safety assessmentevaluation methodology is an important decision that should be carefully considered <u>dueowing</u> to its crucial consequences. This selection This section discusses the capabilities and limitations of SMA,-based SMA, and SPSA²¹ and provides recommendations on the applicability of each assessment methodology to a number of common objectives for existing and new installations. The selected assessment methodology should satisfymeet the following objectives:

- (a) The selected assessment methodology should be adequate for achieving the objective of the seismic safety evaluation in the context of the reasons that motivated the <u>seismic</u> <u>safety</u> evaluation. Paragraphs 2.16 and 2.15 list (a number of these objectives and reasons; are listed in paras 2.16 and 2.15, respectively. This section provides guidance on the applicability of each methodology (i.e., SMA, PSA-based SMA, and SPSA)²² to a number of common objectives for existing and new installations.);
- (b) The selected methodology and its end products should be able to meet the regulatory requirements applicable to the installation $\frac{1}{2}$
- (c) The <u>selected</u> methodology should be capable of demonstrating that the installation will meet the <u>safety</u> requirements <u>describedindicated</u> in paras-1.1–1.1, as applicable to the <u>reasons for the</u> evaluation reasons and <u>the</u> installation type. Requirement 15 of GSR Part 4 (Rev. 1) [1] indicates that both deterministic and probabilistic approaches complement

²² The methodologies presented in this publication are internationally recognized approaches that reflect the current state of practice. Other methodologies may be used in individual Member States in the context of their national regulatory environment. Such latter methodologies are not covered in this publication.



²¹ The methodologies presented in this publication are internationally recognized approaches that reflect the current state of practice. Other methodologies may be used in individual Member States in the context of their national regulatory environment, but these methodologies are not covered in this Safety Guide.

one another and specifies that both approaches be included in safety analysis within a graded approach. This section discusses the capabilities and limitations of each methodology.

3.2.3.3. It is possible that more More than one assessment methodology²³ conmight satisfy the objectives listed in para. 3.1.3.2. In deciding between multiple feasible methodologies, the selection should consider the following should be considered:

- (a) The availability and quality of knowledge and data sources needed to support the execution of the methodology and its technical elements. For example, the for SPSA methodology requires the performance of, site-_specific probabilistic seismic hazard analysis (PSHA) studies analyses need to be conducted, which in turn requirerely on the availability of specific information about seismicity rates and ground motion propagation characteristics from all potential sources within a distance range that can contribute to the seismic hazard of interest at the installation, and the_explicit characterization of uncertainty in these parameters. AFor deterministic seismic hazard analysis only needs, knowledge of this information is only needed for the few rupture sources that dominate the seismic hazard at the installation, and can accommodate a less explicit uncertainty characterization can be accommodated.
- (b) The schedule-requirements for executing the selected methodology.
- (c) The initial and maintenance $cost^{24}$ commitments of the selected methodology.
- (d) The potential added values value achieved in addition to the primary safety evaluation objective, and their alignmenthow that added value aligns with the longer-term strategic objectives of the installation. The Value might be added values through the ability to consider may include usability of use the safety assessment methodology components or end products for other objectives, reusability the ability to reuse or upgradeability of upgrade these components or end products in the future, and the flexibility to

²³ The scope of this document This Safety Guide primarily focuses on seismic safety evaluation that uses the concepts of HCLPF and/or Seismic Fragility for definingseismic fragility to define the seismic margin of the nuclear installation. Alternative methods for seismic safety evaluation that are not predicatedbased on using the use of HCLPF (and/or Seismic Fragilities) for estimating the seismic margin of the installationseismic fragility are not precluded if they are justifiable. In determining the appropriate evaluation methodology to be implemented executed, consideration should be given to the history and characteristics of the site, the level of risk posed by the site specific seismic hazard, the basis of the key safety case claims and objectives, and the national regulatory practice.

²⁴ The maintenance cost is in reference to the levelcost of effort required to periodically updateupdating the SPSA or SMA to keep its results valid over time, for instance, to incorporate updates to seismic hazard, modified or replaced SSCs, facility configuration or operational changes, availability of new data, and improvementor improvements in seismic capacity evaluation methods.

³⁰

accommodate future changes in regulatory requirements over the remaining or anticipated service lifelifetime of the installation.

(e) The <u>fact that the</u> assessment methodology does not need to be the same for all <u>seismie-seismically</u> induced hazards and potential SSC failures. For example, <u>an</u> SPSA methodology may be selected to perform the <u>seismic</u> safety evaluation <u>foronly of</u> vibratory ground motions-<u>only</u>. <u>Meanwhile</u>, <u>while</u> a screening evaluation <u>ean-may be</u> <u>selected to</u> demonstrate that the installation has <u>a</u> sufficiently high <u>seismic</u> margin for the effects of the remaining seismic hazards, <u>that is</u>, <u>This implies</u> that <u>these hazards</u> <u>havesuch a seismic hazard would make a</u> negligible contribution to seismic risk and need not be <u>considered</u> explicitly <u>included</u> in the SPSA.

SEISMIC MARGIN ASSESSMENT

3.3.<u>3.4.</u>The SMA methodology is the least resource-intensive of the three methodologies <u>discussedaddressed</u> in this Safety Guide-and; it is used mainly for existing <u>nuclear</u> installations. <u>It The SMA methodology</u> can be executed using as input a seismic hazard characterization developed using either probabilistic or deterministic approaches. <u>The implementation details</u> <u>of Detailed recommendations on how to implement</u> this methodology <u>should meet the</u> <u>guidelines presented are provided</u> in Section 5.

3.4.3.5. The end product of an-SMA is an installation-level HCLPF capacity, which is based on the HCLPF capacity of two (or more) independent success paths-.

<u>3.5.3.6.</u>The SMA methodology is <u>primarily</u> applicable to the following <u>seismic</u> safety evaluation objectives, and <u>it should otherwise</u> be considered of limited applicability-<u>otherwise</u>:

- (a) Determination of the seismic safety margin higher thanabove a specified level earthquake (e.g. the design basis earthquake) or an aetual<u>a recorded</u> earthquake that affected the installation;
- (b) Demonstration of <u>the</u> seismic robustness of the <u>nuclear</u> installation against cliff edge effects, when robustness is characterized by seismic safety margin;
- (c) Demonstration of <u>a</u> sufficient safety margin to restart operation following the occurrence of a beyond design basis earthquake that <u>may have shut downled to the shutdown of</u> the nuclear installation <u>in additionand potentially</u> to other actions defined in Ref. [19];

- (d) <u>Comparing Comparison of an estimate of installation-level HCLPF capacity to with</u> regulatory expectations;
- (e) Identification of weak links in the credited success paths for the nuclear installation's response to a beyond design basis earthquake event;
- (f) Identification of possible upgrades for SSCs in the success paths to improve the seismic safety margin;
- (g) Comparative safety assessment of a group of nuclear installations benchmarked by seismic safety margin against either (i) the same earthquake effects, (ii) the effects of a common earthquake scenario, or (iii) earthquakes that represent the same level of seismic hazard at each site;
- (ih) Effective communication about the robustness of the nuclear installation to stakeholders, including the public $\frac{1}{2}$
- (ii) Demonstration that <u>the current seismic</u> regulatory <u>seismic</u> requirements are <u>being</u> met for <u>plants whichnuclear installations that</u> were designed without seismic <u>regulatory</u> requirements.

PSA-PROBABILISTIC SAFETY ASSESSMENT BASED SEISMIC MARGIN ASSESSMENT

3.6.3.7. The PSA-based SMA methodology is a hybrid between the SMA and SPSA methodologies. It combines the typically less resource-intensive hazard assessment, fragility, and Boolean logic solution approaches of the SMA methodology with the accident sequence event tree and fault tree analysis from the SPSA. This The PSA-based SMA methodology is used for both new and existing installations. The implementation details of Detailed recommendations on how to implement this methodology should meet the guidelines presented are provided in Section 5.

<u>3.7.3.8.</u>The end products of the PSA-based SMA should be the installation-level HCLPF capacity, and the HCLPF capacities for all accident sequences of interest (i.e. minimal cutsets and the corresponding cutsets²⁵) that can lead to an installation performance-unacceptable

²⁵ A <u>"minimal cut-set" cutset</u> is a combination of events (failures) whose sequence causes the accident to <u>that</u>, should they <u>all</u> occur. Occurrence of all events in the cut-set, is necessary and sufficient for theto result in an accident to take place.
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to safety-<u>performance of the installation</u>. An additional end product may be an estimate of the installation-level full-fragility-<u>curve</u>²⁶ in addition to <u>its-the installation's</u> HCLPF capacity. The <u>sequence-cutset</u> level HCLPF capacities are typically taken to be<u>capacity is</u> the highest <u>SSC</u> HCLPF capacity in <u>each-cut-seta</u> cutset. The sequence level HCLPF capacity is the lowest <u>HCLPF capacity in the constituent cutsets</u>.

3.8.3.9. The PSA-based SMA methodology is applicable to the following <u>seismic</u> safety evaluation objectives in addition to those <u>introduced_listed</u> in para. 3.6, and <u>it</u>-should <u>otherwise</u> be considered of limited applicability-<u>otherwise</u>:

- (a) <u>ComparingComparison of</u> an estimate of installation-level and accident <u>elass-sequence</u> level HCLPF capacities <u>towith</u> regulatory expectations;
- (b) Identification of critical accident scenarios that <u>canmight</u> undermine safety in the <u>nuclear</u> installation's response to a beyond design basis earthquake event, and <u>identification of</u> the weak link(s) in each <u>accident</u> sequence;
- Identification and prioritization of possible upgrades for safety-related SSCs to improve the seismic safety margin;
- (d) <u>ProvidingProvision of preliminary insight toinsights for risk-informed design and resource allocation decisions (e.g. safety classification of SSCs);</u>
- (e) Comparative safety assessment of a group of installations benchmarked by either (i) installation-level seismic safety margin or (ii) sequence-level seismic safety margins against specific accident classes and/or potential consequences.

SEISMIC PROBABILISTIC SAFETY ASSESSMENT

3.9.3.10. The SPSA methodology can only be executed using as input a site-specific seismic hazard characterization developed using probabilistic approaches. The SPSA methodology discretizes the seismic hazard from PSHAprobabilistic seismic hazard analysis into acceleration levels with corresponding annual occurrence frequencies and explicitly convolves²⁷ these frequencies with the installation-level fragility. The installation-level fragility should be constructed by explicitly solving the installation accident sequence. Boolean logic trees are

²⁷ Convolution is a type of mathematical integration. Ref. Reference [11] provides an example of the convolution integral.

²⁶ The installationInstallation-level fragility represents is the conditional probability of facility unacceptable performance of the installation for a given value of the hazard parameter (e.g. peak ground acceleration). It is normally presented as a function of the hazard parameter in the form of a curve. It is commonly referred to as "plant-level fragility' for nuclear power plants. See Section 5 for more details.

solved_using failure probabilities obtained by quantifying accident <u>sequenciessequences</u> associated to with each initiating event. Non-seismic failure rates of SSC and human error probabilities are also taken into consideration in SPSA. This methodology is used for both new and existing installations. The implementation details of Detailed recommendations on how to implement_this methodology should meet the guidelines presented are provided in Section 5. More guidance on the SPSA recommendations on probabilistic safety assessment methodology can be found in IAEA_Safety_Standards_Series_No._general_are_provided in [DS523]_7 Development and Application of Level 1 Probabilistic Safety_Assessment for Nuclear Power Plants-[15].

3.10.3.11. The end products of the SPSA should include the products of the two SMA methodologies, plus-the annual frequency of the installation unacceptable performance of the installation due to seismic hazard, the installation_level fragility curve, the risk importance metrics for accident sequences and components, and the explicit quantification of uncertainties in the computed results.

<u>3.11.3.12.</u> The SPSA methodology is applicable to the following <u>seismic</u> safety evaluation objectives in addition to those <u>introducedlisted</u> in paras. <u>3.53.6</u> and <u>3.8</u>, <u>which should be</u> <u>considered in the methodology selection3.9</u>:

- (a) <u>ComparingComparison of</u> the risk metrics for unacceptable performance (e.g. core damage frequency<u>and</u>, large <u>or</u> early release frequency) to with regulatory expectations;
- (b) Quantification and ranking of relative risk contributions (e.g. of accident sequences and, individual SSCs or human actions) in the installation's as-operated condition;
- (c) Evaluation of risk reduction worth of possible SSC upgrades, procedureprocedural changes, or mitigation strategy implementation;
- (d) <u>ProvidingProvision of</u> quantitative input to risk-_informed design and resource allocation decisions (e.g. impact toon risk from of the safety classification of SSCs);
- (e) Understanding <u>of uncertainty in seismic safety metrics²⁸</u> and incorporation of uncertainty <u>in seismic safety metrics</u> into the <u>seismic</u> safety evaluation conclusions;

²⁸ Uncertainty in the seismic safety metrics is due to the aggregate uncertainty in several factors, e.g. seismic hazard, <u>SSC responses to seismic input, and seismic capacities and failure rates.</u> 34

- (f) Enabling <u>of</u> risk monitoring models that integrate real-_time <u>condition</u>-changes in the <u>condition of the</u> installation (e.g. living <u>PSAprobabilistic safety assessment</u> and digital twin technologies);
- (g) Comparative safety assessment of a group of installations benchmarked by either seismic safety margin or risk metrics.

CONSIDERATIONS ON APPLICATION OF METHOLDOLOGY TO NEW OR EXISTING NUCLEAR INSTALLATIONS

3.12.<u>3.13.</u> The In selecting the most appropriate assessment methodology-selection should be constrained by, the objectives of the seismic safety evaluation and available the information available for each nuclear installation, should be taken into account. The objectives of the seismic safety assessmentevaluation are different for a new installation (see paras 2.13 and _____2.14) and for an existing installation (see paras 2.15–2.17). In addition, there may be substantial differences in the available information available for new installations and for existing installations (see para. 4.1). AData collection for a new installation project will typically face different challenges in collecting data (e.g. collection of site characterization information) will typically entail different challenges from those indata collection for an existing installation. Both aspects, the objectives of the assessment and the available information, should be considered when selecting the most appropriate methodology.

<u>3.13.3.14.</u> The selected methodology should <u>be able to meetenable</u> the applicable regulatory requirements to be met. Regulatory requirements for existing nuclear installations and for new installations are may be different in several-Member States.²⁹.

3.14.<u>3.15. ThePriorities regarding the</u> schedule and cost <u>priorities forof</u> the seismic safety assessmentevaluation should be considered in the selection betweenwhen choosing among multiple feasible methodologies. These <u>schedule and cost</u> priorities and their <u>impact on the final</u> decision-making consequences are typically <u>distinct in a different for</u> new nuclear installation from those in an installations and existing installation, dueinstallations, owing to the constraints of <u>the</u> applicable <u>regulationsregulatory requirements</u> and socio-economic factors.

²⁹ For example, in the United States of America, new nuclear power plant <u>licenselicence</u> applications are required to demonstrate a plant-level HCLPF of at least 1.67 times the ground motion response spectrum that defines the design basis earthquake. This requirement is not applicable to operating nuclear plants, <u>however</u>.

3.15.3.16. The anticipated service lifeoperating lifetime of a new nuclear installation may be different and will typically be significantly longer than the remaining service lifeoperating lifetime of a similar existing installation. This should make As a result, the reusability and shelf life of a more rigorous methodology would be longer for a new installation. Accordingly, the 'return on investment' from performing the more cost extensive SPSA methodology investment is typically higher for a new nuclear installation typically runs longer than for an existing installation, which may be approaching the end of its service life and might justify the selection of the more costly SPSA methodology.
4. DATA COLLECTION AND INVESTIGATIONS FOR EVALUATION OF SEISMIC SAFETY FOR NUCLEAR INSTALLATIONS

DATA AND DOCUMENTATION ON THE DESIGN BASIS

General

4.1. The design basis data and documentation should be collected from all available sources. This <u>compilationtask</u> does not pose special difficulties for new nuclear installations. For existing installations, emphasis should be <u>putplaced</u> on the collection and compilation, as far as <u>possible</u>, of the specific data and information on the nuclear installation that were used at the design stage. It is acknowledged that<u>Although there may be</u> limitations on the quantity and quality of the available original design data <u>may arise</u> for old existing installations. However, the more complete information is collected from the design stage, the less effort and fewer resources will be <u>requiredneeded</u> for the seismic safety evaluation.

General documentation of the for a nuclear installation

4.2. All available general and specific documentation for new and existing <u>nuclear</u> installations <u>relevant to the seismic safety evaluation</u> should be compiled, including the following:

(a) The safety analysis report, preferably the final safety(a) Safety analysis report.

- (b) Codes and standards used for the design of the installation:
 - Standards adopted and procedures applied to specify the nominal properties of the materials used and their mechanical characteristics;
 - (ii) Standards adopted and procedures applied to define load combinations and to calculate the seismic design parameters;
 - (iii) Standards used for the design of structures, components, piping systems and other items, as appropriate;
 - (iv) Standards and procedures usedwhich would have been considered minimum requirements for the design of conventional buildings at the time of the design of the installation, which ought to have been considered minimum requirements.
- (c) General arrangement and layout drawings for structures, equipment, and distribution systems (e.g. piping, cable trays, ventilation ducts).
- (d) Probabilistic safety assessment (PSA) of internal (and external) events, if performed.

- (e) For existing installations, data and information on results and reports of seismic qualification tests for SSCs performed during the pre-operational period, including any information available on inspection, maintenance, and non-conformance reports and corrective action reports. For new installations, <u>the</u> specifications for seismic qualification tests (e.g. required necessary response spectra) maynight be sufficient.
- (f) For existing installations, quality assurance and quality control documentation, with particular emphasis on the as-built conditions for materials, geometry and configuration₇ (for assessing the modifications during construction, fabrication, assembly and commissioning₇), including non-conformance reports and corrective action reports. The accuracy of the data should be assessed.

Specific documentation offor the SSCs included in the seismic safety evaluation

4.3. <u>Specific The following specific information on the original design of the installation, in</u> particular on those SSCs included in the programme for seismic safety evaluation, should be collected, as follows:

- (a) System design:
 - (i) System description documents;
 - (ii) Safety, quality and seismic classification;
 - (iii) Design reports;
 - (iv) Report on confirmation of the functionality of systems;
 - (v) <u>InstrumentationSystem instrumentation</u> and control-of the system, including the general concept, the typetypes of device and how the devices and how they are mounted.
- (b) Geotechnical design:
 - Excavation, structural backfill and foundation control (e.g. for settlement, heaving and dewatering);
 - (ii) Construction of retaining walls, <u>foundations</u>, <u>underground structures</u>, berms or artificial slopes;
 - (iii) Soil-foundation-structure failure modes and design capacities (e.g. estimated settlements, sliding, overturning, uplifting, liquefaction).
- (c) Structural design:

- (i) <u>StressStructural</u> analysis reports for all structures of interest;
- Structural drawings (e.g. structural steel, reinforced and/or prestressed concrete), preferably as-built documentation for existing installations;
- (iii) Material properties (specified and test data);
- (iv) Typical details (e.g. connections).
- (d) Component design:
 - (i) Seismic analysis and design procedures;
 - (ii) Seismic qualification procedures, including test specifications and test reports;
 - (iii) Typical anchorage requirements and types used;
 - (iv) Stress analysis reports;
 - (v) Pre-operational test reports, if any.
- (e) Distribution system design (<u>e.g.</u> piping, cable trays, cable conduits, ventilation ducts):
 - (i) <u>SystemsSystem</u> description documents;
 - (ii) Piping and instrumentation diagrams;
 - (iii) Layout and design drawings of piping and its supports;
 - (iv) Diagrams of cable trays and cable conduits and their supports;
 - (v) Diagrams of ventilation ducts and their supports;
 - (vi) Design Reports reports, including stress analysis reports if available.
- (f) Service and handling equipment (although some of this is non-safety-related equipment, its evaluation may be needed for analysis and study of interaction effects in operational and storage configurations):³⁰.
 - (i) Main and secondaryauxiliary cranes, monorails and hoists;
 - (ii) Fuel handling equipment.

Seismic design basis

³⁰ Although some service and handling equipment is non-safety related, its evaluation may be needed for analysis and study of interaction effects in operational and storage configurations.

4.4. TheTo conduct a seismic safety evaluation, the characterization of the seismic input used for design should be well understood for conducting the seismic safety evaluation. Any discrepancy between the documentation of the seismic hazard assessment performed during the site evaluation studies and the design basis values finally adopted should be identified. This information is essential for determining the reference level earthquake, which will be used to assess in the evaluation of seismic safety margin of the installation. In this regard, the following aspects should be covered:

- (a) Specification of the design <u>basis</u> earthquake <u>level(s) as</u> used for the design and qualification of SSCs [7].(see SSG-67 [8]).
- (b) FreeSite specific free field ground motion parameters in terms of elastic ground response spectra, acceleration time histories or other descriptors, such as the power spectral density.
- (c) Dominant earthquake sourceSeismological parameters used to define representative of the <u>earthquakes that make the largest contribution to</u> seismic input motionshazard, such as magnitude, distance, definition and duration of strong motion. Other parameters, such as the focal mechanism or the source spectral shape, might have been used as well.
- (d) If some structures were designed in accordance with design codes whose design spectra have implicit reductions for inelastic behaviour, the corresponding elastic ground response spectra should be derived to provide a basis <u>offor</u> comparison with the elastic ground response spectra typically used to define the reference level earthquake for the seismic safety evaluation.

Soil-structure interaction, structural modelling and in-structure response details

4.5. Information on soil–structure interaction analysis, modelling techniques, and techniques of structural response analysis used in the design should be collected as follows:

- (a) Soil-structure interaction parameters:
 - The location selected for applying the seismic input ground motion for example, free field surface on top of finished grade, foundation mat level or base rock level (often referred to as the 'control point location/);
 - Soil profile properties <u>applicable to each building or structure on the ground</u>, including soil stiffness and damping properties used in the site-specific response
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analysis, information on the water table variation, and consideration of strain dependent properties;

- (iii) Method to account for uncertainties in soil properties and techniques of soil– structure interaction analysis, for example, envelope of three analyses for best estimate, lower bound, and upper bound soil profiles;
- (iv) Applicability and consideration of seismic wave phenomena in the definition of the input motion. Those should include:, including the definition of seismic input motion typically as a vertically propagating shear wave (typical);, coherency; and wave passage effect.
- (b) Modelling techniques:
 - Modelling techniques and analytical methods used to calculate the seismic response of structures and the in-structure response spectra (floor response spectra);
 - Material and system damping, cut-off of modal damping, frequency dependency of damping;
 - (iii) Allowance for inelastic behaviour, as assumed in the design phase and as implemented during construction.
- (c) Structural analysis and response parameters:
 - (i) One- or two-stage analysis, using coupled or substructure models of soil and structures;
 - (ii) <u>Characterization of the soil foundation system (e.g. by impedance or transfer</u> <u>functions):</u>
 - (iii) Equivalent static analyses of components and structures;
 - (iiiv) Dynamic analysis of components and structures;
 - (iiiv) Natural frequencies and modal shapes, if available;
 - (ivvi) Output of structural response (e.g. structure internal forces and moments, instructure accelerations, deformations-or, displacements);
 - (vii) Foundation response, including overall behaviour such as sliding or uplift;

(viviii) Calculations of in-structure response spectra (floor response spectra), including:

- Damping of equipment;
- Enveloping and broadening criteria, if used.

ADDITIONAL DATA AND INVESTIGATIONS FOR EXISTING NUCLEAR INSTALLATIONS

Current (as-is) data and information

4.6. For an existing nuclear installation, after collecting as manymuch data as is feasible in relation to about the original design basis, as recommended in paras 4.2–4.5, the present current state and actual conditions condition of the installation (i.e. the <u>sa-is2is</u> condition) should be identified ³⁴. The collection of as-is data should cover those selected SSCs that will be considered within the scope of the programme for seismic safety evaluation and that have either a direct effect on system performance or an indirect effect, such as by transmitting earthquake motion from one location to another or by affecting safety related SSCs in case of <u>a-seismically</u> induced failures. It should be also emphasized that the The as-is condition should properly reflect and include the effects of ageing degradation of the installation throughout its operational perating lifetime. Pending and any pending physical or operational modifications should also be recognized so that they can be taken into account in the <u>seismic safety</u> evaluation. When applicable, a sufficient number of samples should be collected on parameters of interest (e.g. concrete strength) to adequately define the variability (e.g. mean and standard deviation).

4.7. If the nuclear installation has been subjected to periodic safety reviews, as recommended in IAEA Safety Standards Series No. SSG-25, Periodic Safety Review for Nuclear Power Plants [20], the reports of these reviews should be made available for the purposes of the seismic safety evaluation.

4.8. If the operating organization of a nuclear installation has implemented an ageing management programme, (see IAEA Safety Standards Series No. SSG-48, Ageing Management and Development of a Programme for Long Term Operation of Nuclear Power Plants [20]), any outputs from it (e.g. condition assessment, periodic inspection reports) that identify the as-is condition should be made available for the purposes of the seismic safety evaluation. If some SSCs (e.g. active equipment) are not be-covered under an ageing

³⁴ Any seismic safety evaluation to be performed for an existing nuclear installation should be made by considering the state of the installation at the time the assessment is performed. This condition of the installation is denoted the 'as-is' condition. Consequently, one of the first and more important steps of the programme for seismic safety evaluation is to collect all the necessary data and information to provide a complete representation of the actual situation of the installation.



management programme, but <u>underby</u> some other programme (e.g. <u>monitoring of the</u> <u>effectiveness of</u> maintenance <u>rule programme</u>), the related documentation should also be made available for the purposes of the seismic safety evaluation.

4.9. A critical review of all available as-built and pre-operational documentation (e.g. reports, drawings, photographs, film records, reports of non-destructive examinations) should be performed. For this purpose, a preliminary screening walkdown should be earried outconducted to confirm the documented data and to acquire new, updated information. During this walkdown, data about any significant modifications and/or upgrading, upgrades and/or repair measures that were performed over the lifetime of the nuclear installation should be collected and documented, including any reports on ageing effects. The judgement abouton how significant a modification would need to be in order to have an impact on the seismic response and capacity of the installation should be made by experts on the evaluation of <u>in</u> seismic capacity evaluation.

4.10. Special attention should be paid to requirements, procedures and non-conformance reports for construction and/or assembly related to the following:

(a) Slopes, excavation and backfill;

- (b) SSCs not accessible for inspection;
- (c) Field_routed items (e.g. piping, buried piping, cable trays, conduits, and-tubing);
- (d) Installation of non-safety-related items (e.g. masonry walls, shielding blocks, room heaters, potable water lines-and, fire extinguishing lines, and-false ceilings);
- (e) Separation distances or clearances between components;
- (f) Field-tested items;
- (g) Anchorages.

Recommended investigations: soil data

Investigation of subsoil data and earthquake experience

4.11. To perform reliable and realistic site-_specific seismic response analysis, data on the static and dynamic material properties of soil and rock profiles should be obtained. For an existing installation, if these data were obtained at an earlier stage (e.g. during the design stage), they should be reviewed for adequacy with regard to current methodologies. In this respect the following should be taken into account:

- (a) Appropriate ranges of <u>the</u> static <u>valuesproperties</u> and dynamic <u>values for the</u> <u>geodynamic</u> properties, <u>which</u> <u>that</u> account for <u>the</u> site specific geotechnical characteristics, <u>and their variability</u> should be available for use in the <u>programme for</u> seismic safety evaluation.
- (b) For ground materials, the density and low strain properties (normally in situ measurements of compressional, P, and shear, S, wave velocities), laboratory measurements of three-axis static properties, and, if possible, dynamic properties and material damping ratio should be available.
- (c) As a function of depth, the variation of dynamic shear modulus values and damping values with increasing strain levels should be available. Strain dependent variations in ground material properties may be based on generic data if ground materials are properly correlated with the generic classifications.
- (d) For hard rock layers, variation of properties with increasing strain levels may usually be disregarded.

In operating nuclear installations, the performance of it might be difficult to perform soil investigation campaigns might encounter implementation difficulties. In such cases, as much data should be gathered as is practicable, but judgement may might need to be needed, supported by all practically achievable gathering employed in the collection of data. In any case, However, the substitution of physical data by judgement should be avoided to the maximum extent possible.

4.12. Information on the location of the local watergroundwater table and its variation over a typical year should be obtained.

4.13. For the various stages of site investigation, design₇ and construction, other data may be available from non-typical sources, such as photographs, notes₇ and observations recorded by operations staff or others. These data should be evaluated in the light of their source and method of documentation. To the extent possible, the collection of such data should be carried out in compliance with the recommendations provided in NS-G-3.6 [10].

4.14. All available information relating to actual earthquake experience at the site or at other industrial installations in the region should be obtained. Special attention should be paid to earthquake-_induced phenomena such as river flooding due to dam failure, coastal flooding due to tsunami, landslides, and liquefaction.

Recommended investigations: Investigation of data on building structures

4.15. The as-is concrete classes used for the construction of the safety related structures of the nuclear installation should be verified on the basis of existing installation_specific tests and industry standards for concrete. Destructive and non-destructive testing_methods may be used $\frac{32}{2}$. The as-is data collected, <u>— rather than the nominal design data</u> should be used for further analyses and capacity evaluations<u>—rather than the nominal design data</u>. If there is significant deviation from the design values, the cause of this deviation and its consequences should be investigated.

4.16. The actual material properties of the reinforcing steel should be used in the evaluation. Material properties should be available from existing test data. If not, reliable methods of destructive and non-destructive testing should be used. The information on the reinforcing steel should include both mechanical properties and detailing (e.g. size of reinforcing bars, placement, geometric characteristics, concrete cover, distances between bars). For the evaluation of the overall capacity of a structure, the properties of all significant load bearing members should be evaluated. Other <u>easesexamples of</u> where detailing of the reinforcement may be important include, for example, penetrations and anchorage of large components.

4.17. Although ageing effects are usually estimated in a separate projectseparately, in the seismic safety evaluation, at a minimum, the survey of a concrete building should, at a minimum, include visual examination for cracks, effects of erosion/corrosion and surface damage, the degree of carbonizationcarbonation, the thickness of concrete cover, the current prestress of tendons and the degree of degradation of below ground foundations due to, for example, chlorides or other corrosive contaminants present in groundwater.

4.18. A sample survey should be <u>madeperformed</u> to verify the geometrical characteristics of selected structural members. The number of samples collected should be statistically significant to allow for the accurate computation of sample statistics (e.g. sample mean<u>and</u>, sample standard deviation).

4.19. An important element of the <u>seismic safety</u> evaluation is the verification of realistic nonseismic loads (e.g., live and dead loads) and possibly the new assessment of loads, other than seismic loads, that will be used in the seismic safety evaluation. Usually, both the dead and the live loads in the as-is condition <u>differdeviate</u> from those used in the original design. The deviations should be carefully examined and documented.

³² Non-destructive methods alone are usually not sufficient for <u>reliably</u> establishing concrete strength with reliability. 45

Recommended investigations: Investigation of data on piping and equipment

4.20. If design information is inadequate for piping, equipment, and their supporting structural systems is insufficient or not available, analysis and/or testing should be performed to establish their dynamic characteristics and behaviour. A representative sample may be sufficient.

5. <u>EVALUATION OF</u> SEISMIC SAFETY <u>ASSESSMENT</u> FOR NUCLEAR INSTALLATIONS, <u>WITH A FOCUS ON NUCLEAR POWER PLANTS</u>

ASSESSMENT OF SEISMIC HAZARDS FOR NUCLEAR INSTALLATIONS

Seismic hazard assessment approach

5.1. Site specific <u>seismic</u> hazard <u>analysis</u> should preferably be used to characterize the <u>seismic hazard and</u> reference level earthquake for the seismic safety evaluation (see para. 2.22). The seismic hazard assessment may be performed using a probabilistic or a deterministic approach, or a combination of both. A probabilistic approach should be used to develop the reference level earthquake for an SPSA. A deterministic approach mayshould be used to develop the reference level earthquake for an SMA and a combination of deterministic and probabilistic approaches for PSA-based SMA.

5.2. The PSHAProbabilistic seismic hazard analysis should include a probabilistic characterization of ground motions that can be produced at the installation site by all seismic sources within the regional seismotectonic model, in accordance with (see SSG-9 (Rev. 1) [7]). Ground. The ground motion characterization should be performed for the range of annual frequencies requiredneeded to meet the regulatory requirements and to achieve the objectives of the seismic safety evaluations. Deaggregation of the PSHAprobabilistic seismic hazard analysis results should be performed attfor the reference level earthquake to identify the dominant seismic sources, that is, those that havemake the largest contributions to the hazard.

5.3. The Deterministic Seismic Hazard Analysis (DSHA)seismic hazard analysis should include determination of ground motions that the dominant seismic sources within the regional seismotectonic model are capable of producing at the installation site. The ground motions should be determined in accordance with SSG 9 [7], considering the maximum potential maximum magnitude of each source, the closest associated distance to the site, and an appropriately high confidence level to account for variability due to epistemic uncertainty and aleatory variability in the source model, ground motion prediction model, and site conditions (see SSG-9 (Rev. 1) [7]). The dominant seismic sources in a deterministic seismic hazard analysis should be identified by careful review of the seismotectonic model, as recommended in SSG-9 (Rev. 1) [7], in the absence of deaggregation data from a probabilistic seismic hazard analysis.

5.4. The dominant seismic sources in a DSHA should be identified by careful review of the seismotectonic model, as recommended in SSG-9 [7], in the absence of deaggregation data from a PSHA. Dominant sources mayDominant sources might not be the same for the different ground motion parameters and other seismic hazards (see para. 2.19). For sites located in a region of low to moderate seismicity, low-frequency ground motion accelerationsmotions can be dominated by distant high-__magnitude sources, while high-__frequency ground accelerationsmotions are often dominated by diffuse seismicity, that is, by_nearby moderate magnitude sources. GeologicalGeotechnical failures are primarily caused by low-_frequency ground motions, while the dominant sources for concomitant phenomena hazards are phenomenon specific.

Development of the reference level earthquake

5.5. The reference level earthquake is the seismic hazard realization at which the responses and capacities of the SSCs identified for the seismic safety <u>assessmentevaluation</u> should be explicitly <u>evaluatedassessed</u>. A reference level earthquake is necessary for technical consistency in the <u>seismic</u> safety evaluation, considering that several important dynamic response parameters depend on the seismic excitation level, including the following:

- Damping, which depends on the extent of shaking-_induced cracking in concrete structures and slip or other connection deformations in metallic structures;
- (b) Geotechnical material properties and physical integrity, <u>which</u> exhibit degradation as the shaking level increases;
- (c) The potential for the <u>occurrence of</u> geotechnical failures whose characterization is necessary to evaluate the geological stability of the site (see para. 2.19-((a))), which typically depends on the shaking level.

5.6. The reference level earthquake should be defined for the vibratory ground motion hazard, using response spectra that characterize horizontal and vertical ground <u>accelerationmotion</u> components at the site. For other seismically induced hazards (e.g. fault displacement), <u>development of reference</u> parameters should be <u>performeddeveloped</u> on a case-specific basis if these hazards cannot be screened out in accordance with para. 5.11.

Characterization of vibratory ground motions

5.7. For SMA and PSA-based SMA-evaluations, the reference level earthquake may be set according to several criteria and should be in accordance with the objectives of the <u>seismic</u>

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safety <u>assessmentevaluation</u> (see paras 3.6 and $\frac{3.7}{3.8}$) and <u>the</u> available hazard assessment information-(see paras 5.1 - 5.4). These criteria include the following:

(a) A scaled spectrum of the original design basis earthquake;

(b) A scaled spectrum or broadened spectrum of an earthquake that affected the installation;

(c) A generic spectrum or suite of spectra (e.g. used in certification of a standard design);

(d) A scaled site_specific spectrum for a specified earthquake scenario (e.g. para. 5.3);;

(e) A site-specific spectrum for a specified uniform hazard of exceedance (e.g. para. 5.2);

(f) A generic or site-specific spectrum determined by the regulatorregulatory body.

5.8. When the reference level earthquake is not based on current site-_specific hazard assessments, as in paras-5.7(a)-5.7(c), the corresponding spectra should be compared to the site-specific deterministic or uniform probabilistic hazard spectra (see para. 5.1) to develop an understanding of the resulting seismic safety margin of the <u>nuclear</u> installation in a site specific context.

5.9. For SPSA-evaluations, the reference level earthquake spectrum at each frequency should be set to spectral acceleration levels that contribute most significantly to the resulting seismic risk and <u>that</u> have comparable, but not necessarily equal, annual probabilities of exceedance. <u>This determination may involve an iterative process</u>. The following considerations should be observed in the reference level earthquake for SPSA:

- (a) The selected reference level earthquake spectrum shape should result in low sensitivity of the computed seismic risk to the selection of the ground motion hazard parameter for the SPSA (e.g. peak ground acceleration or spectral acceleration at selected frequencies);
- (b) Because prior to performance of the SPSA, Since the relative contributions of ground motion levels to seismic risk can only be estimated <u>before SPSA is performed</u>, the appropriateness of the reference level earthquake based on this estimation should be confirmed (e.g. using sensitivity studies) after completion of the SPSA-or, and addressed if it is found to be questionable (e.g. using sensitivity studies)-inappropriate.

Characterization of other seismically induced hazards

5.10. <u>Characterization of the The</u> reference level earthquake parameters for other seismically induced hazards is only <u>necessaryneed to be characterized</u> for those hazards that cannot be

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screened out of explicit <u>assessment in the seismic safety</u> evaluation-in the safety <u>assessment</u>. <u>Screening of non. Non</u>-vibratory ground motion hazards and concomitant phenomena (<u>see</u> para. 2.19) should be individually <u>performedscreened</u> for each hazard and credible phenomenon.

5.11. <u>Screening should be performed basedHazards may be screened out</u> on <u>the basis of</u> one of the following two criteria:

- (a) Credibility: Occurrencethe occurrence of the screened hazard at the site with a severity that <u>challengeswill challenge</u> the <u>installationinstallation's</u> safety is practically impossible, or its annual probability of occurrence is too low compared to the reference level earthquake for vibratory ground motions (e.g. <u>the</u> fault displacement hazard is screened out <u>dueowing</u> to <u>an</u> absence of capable faults in close vicinity <u>ofto</u> the nuclear installation, <u>or;</u> liquefaction is screened out <u>because</u> soil deposits are so dense and <u>ground waterthe groundwater</u> table is so low that liquefaction <u>maywould</u> only occur at incredibly high vibratory ground motions).
- (b) Consequence: Potential the potential occurrence of the screened hazard has no consequence on the safety of the nuclear installation <u>dueowing</u> to physical features or reliable mitigation measures (e.g. river flooding due to upstream dam failure leads to an upper bound water line elevation at the site that does not challenge the external flood design basis of the installation).

5.12. For non-vibratory seismic hazards that cannot be screened out, the reference parameters for SMA and PSA-based SMA evaluations should be determined on a hazard-_specific basis_ considering the criteria adopted for the reference level earthquake spectrum (see para. 5.7) and the hazard assessment approach (see para. 5.1). These reference parameters for explicit evaluation have logical correspondence with the reference level earthquake spectrum but do not necessarily correspond to the same annual probabilities of exceedance at the same confidence level as the vibratory ground motion. Options for determining these parameters include the following:

- (a) Ground motion parameters developed using deterministic <u>seismic</u> hazard <u>assessmentanalysis</u> in accordance with paras 5.3 and 5.4. The reference <u>level</u> parameters should be scaled by an appropriate margin based on the reference level earthquake spectrum.
- (b) Ground motion parameters developed using probabilistic <u>seismic</u>hazard <u>assessmentanalysis</u> in accordance with para. 5.2 and prediction equations specific to
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these parameters ³³. The reference<u>level</u> parameters should correspond to annual probabilities of exceedance similar to those of the reference level earthquake spectrum at an appropriately high confidence level to account for uncertainties in the geotechnical evaluation.

(c) Ground motion parameters developed using geotechnical evaluations of the site response at the reference level earthquake for vibratory motion (e.g. slope deformation evaluation using the reference level spectrum as input motion). The reference-level parameters (e.g. slope displacement) should correspond to an appropriately high confidence level to account for uncertainties in the geotechnical evaluation.

5.13. For non-vibratory <u>seismic_hazards</u> that cannot be screened out, the reference <u>level</u> earthquake parameters for SPSA <u>evaluations</u>-should be determined using <u>a</u>-probabilistic <u>seismic</u> hazard <u>assessment_approachanalysis</u> (see para. 5.2). The determination of ground motion parameters in the range of annual exceedance frequencies of interest may be performed by direct prediction (e.g. see para 5.12-((b)) or indirect prediction (e.g. see para. 5.12-((c))). In any case, the epistemic uncertainty and aleatory variability <u>should be incorporated_</u> in the <u>assessment_analysis</u> approach for each hazard <u>should be incorporated_</u>. The reference <u>level</u> parameters should-correspond, at a minimum, <u>correspond</u> to annual probabilities of exceedance similar to those of the reference level earthquake spectrum. However, <u>dueowing</u> to <u>typically</u> strong nonlinearities associated with geotechnical failure modes, and their potential to cause site-wide cliff edge effects, multiple earthquake levels, especially above the reference level, should be explicitly used in developing the fragility functions associated with the corresponding SSC failures.

5.14. For concomitant phenomena that cannot be screened out in accordance with para. 5.11, the reference <u>level</u> earthquake parameters should be determined on a case-specific basis. These phenomena may be triggered by earthquake ground motions occurring at sites with significantly different subsurface properties or located far away from the <u>nuclear</u> installation, and their correlation with the reference level earthquake ground motions at the site <u>requiresneeds</u> specific evaluation.

³³ Ground motion prediction equations for most non-vibratory ground motion parameters are typically at an earlier stage of technical evolution than those for vibratory ground motion parameters, and <u>are typically</u> not as <u>commonlywidely</u> available or <u>as</u> reliable <u>as</u>, those for vibratory ground motions.

IMPLEMENTATION GUIDELINES COMMON TO ALL <u>SAFETY ASSESSMENT</u> METHODOLOGIES FOR EVALUATION OF SEISMIC SAFETY FOR NUCLEAR INSTALLATIONS

Scope of the seismic safety assessmentevaluation

5.15. <u>A multidisciplinaryAn</u> expert team <u>composed of comprising</u> systems engineers, <u>operationsoperating</u> personnel, and seismic capability engineers should collectively determine the scope of the seismic safety <u>assessmentevaluation</u>. A typical <u>assessmentevaluation</u> team should have <u>3 - 5three to five</u> members._³⁴-. The <u>first</u>-four steps involved in <u>this</u> <u>determinationdetermining the scope</u> of the <u>scopeseismic safety evaluation</u> are described in paras 5.16 to __5.19. These steps are fundamentally the same for <u>all three assessment methodologies</u> <u>discussed in Section 3SMA, PSA-based SMA and SPSA</u> and differ only in <u>their</u> implementation details <u>as noted where applicable to each methodology later in this Section.(see paras 5.38-5.65).</u>

5.16. The first step in determining the scope of the seismic safety evaluation should be identifyingto identify the safety functions to be fulfilled in order to control the progression or mitigate the consequences of an accident to <u>achieve</u> an acceptable end state if the <u>nuclear</u> installation experiences a <u>beyond design basisan</u> earthquake. These safety functions and acceptable accident end states should be in accordance with the regulatory framework and the <u>relevant IAEA</u> safety requirements for the nuclear installation.³⁵

5.17. The second step in determining the scope <u>of the seismic safety evaluation</u> should be to establish agreement on the following <u>defining conditions for the safety assessmentaspects</u>:

(a) Establishing the The initial conditions of the nuclear installation to be considered at the time of the earthquake. This Establishing these initial conditions includes, for example:
 (i) definition of whether defining which modes of operation are to be considered for the installation is in normal operating mode or in another mode (e.g. shutdown); (ii) definition of defining what constitutes normal operating conditions for the installation systems and their components; and (iii) determining whether a seismic seismically induced abnormal condition (e.g. loss of off-site power, small loss of coolant accident)

³⁴ The assessmentevaluation team selection process is reviewed in Ref. [11]. The team is expected to consist of both staff from the nuclear installation and consultants.
³⁵ For nuclear power plants, Requirement 4 inof SSR-2/1 (Rev. 1) [3] lists the fundamental safety functions as: (i) control

³⁵ For nuclear power plants, Requirement 4 ino! SSR-2/1 (Rev. 1) [3] lists the fundamental safety functions as: (i) control of reactivity; (ii) removal of heat from the reactor and from the fuel store; and (iii) confinement of radioactive material, shielding against radiation and control of planned radioactive releases, as well as limitation of accidental radioactive releases. 52

should be triggered and considered to occur <u>concurrent_concurrently</u> with or following earthquake <u>induced</u> shaking (e.g. loss of off site power or small loss of coolant <u>accident)</u>.

- (b) DefiningDefinition of the safety-related functions and corresponding systems that are credited in achieving thean acceptable end states identified in para. 5.16.state. The SMA methodology focuses on defining a subset of functions and systems necessary to achieve a determined number of success paths (typically two) to an acceptable end state. The PSA-based SMA and SPSA methodologies broaden their have a broader focus to include systems and that includes functions and systems whose failure might lead to the progression of an accident to an unacceptable end state.
- (c) <u>IdentifyingIdentification of</u> operator actions that are credited in the <u>seismic</u> safety evaluation. These actions should be established in the emergency procedures.
- (d) Availability and credit to take forof any non-safety related emergency response and mitigation systems-that are not safety related. This may, and account to be taken of them. These systems include mobile alternative resources (such as supplies of e.g. water, compressed air, and mobile electrical power supplies) stored on the site, that are located and maintained in such a way as to be functional and readily accessible when needed in postulated emergency conditions.
- (e) Availability and credit to take forof outside assistance, and account to be taken of it. The type of assistance, response time, and conditions for availability of outside assistance should be established in the safety procedures and agreed upon with the regulatory body.

5.18. The third step in determining the scope <u>of the seismic safety evaluation</u> should be to prepare a list of selected SSCs³⁶ for seismic capability evaluation. Paras₇ 5.20–5.22 provide recommendations on this process.

5.19. The <u>fourth and final step in determining the scope of the seismic safety evaluation</u> should be to perform a seismic evaluation walkdown. <u>Paragraphs (see paras 5.23–5.33 provide recommendations on this process.</u>). For a new nuclear installation, the walkdown may be

³⁶ The term 'selected SSCs' is used in this Safety Guide to mean those SSCs that are of interest to thein SMA or SPSA. ElsewhereIn other literature, the terms 'safe shutdown equipment list' (SSEL) and 'seismic equipment list' (SEL) haveare commonly been used with a similar meaning. The term, but 'selected SSCs' is used here since required SSCs include more implies a broader meaning than just equipment.



replaced with a virtual review³⁷ (to the extent <u>practicalpracticable</u>) followed by a confirmatory walkdown after construction of the installation is finished.

DevelopmentPreparation of the list of selected SSCs list

5.20. The <u>list of selected SSCs list should be developed prepared</u> jointly by the expert multidisciplinary team. This selection should be based on the following considerations and confirmed by a systems walkdown (see para. 5.21);) The following SSCs should be included in the list:

- (a) Inclusion of SSCs necessary for the safety-_related systems identifieddescribed in para. 5.17(b) to fulfil their safety functions. These SSCs are not limited to front-_line and support safety systems, but include instrumentation and control equipment, cable trays, passive elements, and other distribution systems.
- (b) Inclusion of other-SSCs whose seismic-seismically induced response or damage could interact withmight physically affect one or more of the SSCs other SSCs (e.g. through falling, impact, fire, flood or spray) and interfere with their the ability of those other SSCs to fulfil their safety function (e.g. falling, impact, fire, flood, and spray hazards);functions;
- (c) Inclusion of SSCs whose seismic-seismically induced damage maymight impede the operator actions identifieddescribed in para. 5.17(c) (e.g. by physically injure operators or blockinjuring operating personnel, blocking their entry, egress, or exit, or preventing their use of tools needed to executetake actions);
- (d) Inclusion of SSCs necessary for post-earthquake emergency procedures credited in achieving an acceptable end state, for example, the mitigation systems identifieddescribed in para. 5.17(d);
- (e) <u>Inclusion of SSCs whose seismic seismically</u> induced damage <u>maymight</u> impede the arrival or deployment of the outside <u>help identifiedassistance described</u> in para. 5.17(e);
- (e) <u>Inclusion of the structures(f)</u> Structures that house or support the identified SSCs;

³⁷ A virtual review is such that the 3Da review of a three dimensional model of the installations is displayed directly in he VR space, and some elements of the seismic walkdowns. nuclear installation. 54

- (g) Inclusion of SSCs that represent unique features of the installation from a seismic safety perspective (e.g. an_SSC related to the credible and consequential concomitant phenomena described in para. 5.14)-;);
- (h) SSCs needed during identified design extension conditions, if not already included above.

5.21. A systems walkdown should be performed for existing nuclear installations-<u>(see Ref.</u> [11]). For new installations, a virtual review should be performed of the available design should be performed to the extent practical. This practicable. The systems walkdown should have the following objectives:

- (a) To confirm the completeness and consistency of the list of selected SSCs listas compared with the as-built systems configuration;
- (b) To familiarize the seismic capability engineers with the as-built configuration, conditions, and apparent seismic robustness or vulnerability of the $SSCs_{72}$
- (c) To investigate the surrounding areas to identify potential sources of seismic-seismically induced interactions with the required selected SSCs;
- (d) To ensure that the credited operator travel paths are compatible with plant operating procedures, and:
- (a)(e) To verify potential assumptions used to justify including <u>elements in</u> or screening <u>elements them</u> out of <u>the scope of the seismic safety assessmentevaluation on the basis of their credibility and the consequence(s) of their failure (see para. 5.11).</u>

5.21.5.22. The list of selected SSCs list prepared according to paras 5.20 and 5.21 should include all the SSCs that belong in the success path or logic tree model for the acceptable end state(s) of the nuclear installation. Several SSCs on this list may be removed from explicit seismic capability evaluation if qualitative review indicates that they have either: (ia) significantly low seismic capacities and should be assumed to fail in an earthquake³⁸. These screening decisions should be confirmed by observation in the seismic evaluation walkdown

³⁸ It is recommended SSCs that can be assumed to be seismically rugged demonstrate seismic capacities that significantly exceed the threshold at which they might contribute to the risk of the nuclear installation. This capacity is sometimes referred to as the 'screening level capacity'. These SSCs need not be explicitly evaluated. It is recommended, however, that seismically rugged SSCs be retained in the plant response logic model and assigned nominally high capacities, rather than removing thembe removed from the logic model altogether.



(see para. 5.23). The <u>list of selected SSCs-list</u> should be refined during the walkdown and finalized as part of the walkdown documentation (see para. 5.33).

Seismic evaluation walkdown

5.22.5.23. Seismic evaluation walkdowns are one of the most significant components of the seismic safety evaluation in the SMA and SPSA methodologies. They are often referred to as 'seismic capability walkdowns' in the context of SMA approaches-and 'seismic fragility walkdowns' in the <u>context of SPSA-approach</u>. For <u>existingnew</u> nuclear-installations, they should be performed after completion of the selected SSCs list. For new installation designs that have not been constructed, walkdowns should be performed after completed to verify consistency between the as-built conditions and the as-designed conditions that were used in the <u>seismic safety assessment basedevaluation</u> on <u>the basis of virtual review</u> (see para. 5.21)5.19) and to observe any installation or site specific features. It is important that all design features used for the seismic <u>assessmentsafety evaluation</u> be verified in the as-built installation or <u>___and</u> any deviations addressed <u>___</u> in order for the <u>safety assessmentevaluation</u> to be valid. The final safety analysis report should incorporate any resulting updates to the <u>seismic safety analysis report should incorporate any requirements (see SSG-61 [13]-).</u>

5.23.5.24. Each The seismic evaluation walkdown team should include qualified seismic capability engineers, at least one systems engineer, and at least one installation operator, and member of operating personnel; it may include support personnel as necessary ((e.g. for maintenance, operations, systems, and or engineering), support) as necessary. The seismic capability engineers should have sufficient experience in the seismic analysis, design and qualification of SSCs for resisting earthquakes and other loads arising from normal operations, accidents, and external events. One team member should be familiar with the design and operation of the SSC being walked down.

5.24.<u>5.25.</u> The <u>scope of the</u> walkdown <u>scope</u>—should be defined to <u>covermeet</u> the <u>requirementsneeds</u> of the selected safety <u>evaluationassessment</u> approach within the <u>assessment</u> conditions defined in para. 5.17. The <u>purposepurposes</u> of the seismic evaluation walkdown typically <u>includesinclude</u> the following:

- (a) To collect information that can be used in refining the <u>list of selected SSCs-list;</u>
- (b) To observe and record the current as-built condition of <u>selected</u> SSCs included on the list;
- (c) To verify the screening of SSCs based on very low or very high seismic capacities;

- (d) To identify conditions in these SSCs, <u>or in their</u> anchorage or their configuration (e.g. known or suspected seismically vulnerable details), for consideration in their seismic capacity evaluation;
- (e) To identify the realistic failure modes of each SSC that may prevent <u>achievingthe</u> <u>achievement of</u> an acceptable end state;
- (f) To collect key data such as dimensions that <u>maymight</u> be <u>requiredneeded</u> in <u>seismic</u> capacity evaluations;
- (g) To identify SSCs that maywhose failure might result in previously unidentified seismic spatial interactions (see paras- 5.20(c), 5.20(d);) and 5.20(e)) not previously identified;)), and to collect the necessary information to identify their relevant failure modes, the failure consequences, and the affected SSCs;
- (h) To identify and report 'seismic housekeeping' itemsmatters that can be easily addressed by the <u>nuclear</u> installation <u>operating organization</u> to reduce obvious vulnerabilities, such as temporary or left-in-place equipment that <u>maymight</u> result in seismic interactions (e.g. scaffolding, ladders, carts), missing fasteners, unsecured light fixtures, and unrestrained stored items.

<u>5.25.5.26.</u> The <u>seismic</u> evaluation walkdown process should include preparatory activities, a preliminary walkthrough, <u>development of a walkdown plan</u>; <u>and</u> walkdown guidance, <u>performance of detailed seismic evaluation</u> walkdowns, post-walkdown activities and <u>preparation of documentation</u>.

5.26.5.27. Preparatory The preparatory activities for the <u>seismic evaluation</u> walkdown should be performed to <u>servefor</u> the following purposes:

- (a) <u>Plant familiarization thoughTo familiarize the walkdown team with the nuclear</u> <u>installation through the</u> review of systems diagrams, layout and other drawings, previous seismic evaluations, and available-documentation from prior walkdowns;
- (b) <u>AssemblingTo create</u> a database of selected SSCs.<u>SSC entries should include</u> <u>containing</u> the data available prior to the walkdown-and, which will later be populated <u>later by with the</u> data collected during the walkdown;
- (c) <u>ReviewingTo review</u> the <u>list of</u> selected SSCs list for completeness;
- (d) <u>ReviewingTo classify</u> the selected SSCs <u>on the list for groupings of similar SSCs by type</u> and their location;

- (e) <u>IdentifyingTo identify</u> SSCs and <u>the areas that may require with</u> special access <u>needs</u> and/<u>or</u> safety requirements and protection measures;
- (f) IdentifyingTo identify selected SSCs and areas for the preliminary walkthrough (see para. 5.28);
- (g) <u>Identifying To identifying any</u> access and training <u>requirements forneeds of</u> the walkdown team.

5.27.5.28. The objective of the preliminary walkthrough is <u>for the walkdown team</u> to gain familiarity with the key areas of the <u>nuclear</u> installation and <u>with</u> the general configuration and construction quality of its SSCs in order to facilitate the development of the walkdown plan. The <u>preliminary walkthrough should include the seniorkey</u> members of the walkdown team. It <u>should participate in the preliminary walkthrough. They</u> should focus on observing SSCs which do not needwith no special access requirementsneeded, confirming <u>the</u> consistency of the information obtained fromduring the preparatory reviewactivities (see para. 5.27) with the asbuilt conditions, and identifying <u>any</u> access requirementsneeds and <u>similarity</u> considerations for SSCs <u>similar to one another that were</u> not previously identified in the preparatory activity activities.

5.28.5.29. A detailed walkdown plan and schedule should be prepared and shared with the <u>nuclear</u> installation <u>operating organization</u> ahead of the walkdown. The walkdown plan should specify the following:

- (a) <u>TheList of selected SSC list,SSCs, their</u> locations on layout drawings, <u>andtheir</u> classification by SSC type and general location, and a description of the typical observation activities to be conducted;
- (b) <u>ListsList</u> of similar SSCs-and, identifying the lead items for detailed walkdowns or and other items for confirmatory walkbys³⁹; (see para. 5.31);
- (c) Estimated time required needed for walkdowns and walkbys of typical the various SSC classes;
- (d) List of SSCs with<u>that need</u> special access requirements and the support requested from the installation personnel (e.g. de-energizing <u>of</u> active equipment to examine internals,

³⁹ A <u>*walkby</u> is a brief, non-detailed walkdown with less extensive documentation, for instance, to confirm that an SSC is <u>identicalsimilar</u> to another SSC that has <u>already</u> been walked down and <u>that it</u> is free from potential spatial interaction concerns.

opening <u>of</u> equipment enclosures to observe anchorage, authorization for access to areas with high radiation levels or contamination, escorted access to high-_security areas);

- (e) Identification of areas in the installation where walkdowns of distribution systems and operator travel paths will be performed;
- (f) Identification of the <u>primarykey</u> members <u>onof</u> the walkdown team and confirmation of <u>requiredtheir</u> access <u>needs</u> and training credentials;
- (g) Identification of <u>the</u> necessary safety and protection measures for the walkdown team members.

5.29.5.30. Before executing the walkdowns, project a seismic evaluation walkdown is performed, specific guidance should be prepared, shared with, and reviewed by the seismic capability engineers on the walkdown team. The objective of this guidance should be to maximize the execution consistency inamong multiple walkdowns and the quality of the data collected for the subsequent evaluations. This guidance should include the following:

- (a) Criteria for capacity screening and ranking 40 ;
- (b) Class_specific actions for typical SSC classes (e.g. verifyverification that batteries are vertically restrained);
- (c) Actions for specific SSCs, typically informed by <u>the preparatory workactivities</u> and <u>preliminary</u> walkthrough (e.g. <u>measuremeasurement of</u> the as-built distances across specific building interfaces);
- (d) Actions for walkby review of similar components;
- (e) Criteria for assessing spatial interaction concerns (i.e. principally falling⁴¹ and impact⁴² hazards) and identification of known or suspected concerns to be examined;
- (f) Criteria for assessing seismic-seismically induced fire and flood interaction concerns and foridentification of known or suspected concerns to be examined;

⁴⁰ Capacity ranking assigns involves assigning a qualitative rank to each SSC based on the walkdownbasis of the seismic evaluation walkdown to prioritize the allocation of technical effort in subsequent seismic evaluations. A typical ranking system includes five grades: <u>Low -low (seismically deficient, Medium -)</u>, medium (may be governed by failures external to the SSC design (e.g. related to anchorage.or interaction). <u>High-)</u>, high (likely governed by failure of the SSC design, <u>Rugged-)</u>, rugged (very high seismic capacity₁), and <u>Unknown-unknown</u> (needs additional review.).

⁴¹ A common example isof a falling hazard is the collapse of masonry walls located next to selected SSCs.

⁴² A common example isof an impact hazard is the impact on electrical cabinets containing chatter-sensitive devices by adjacent SSCs or debris.
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- (g) <u>ProcedureProcedures</u> for area-_based or<u>and</u> sampling-_based walkdowns (e.g. of distribution systems);
- (h) Procedure for <u>walking downwalkdown of</u> operator travel paths;
- Procedure for resolving potential-in-process refinements to refinement of the list of selected SSCs list and addressingin order to add or remove SSCs that get added to or removed from the final list;
- (j) <u>InformationProcedure for information</u> collection foron applicable geotechnical failure modes (e.g. measurements to allow <u>evaluatingevaluation of</u> the liquefaction settlement capacity of a piping run);
- (k) Instructions on documentation.

The appendix to this Safety Guide provides seismic failure mode considerations specific to different types of SSCs, which should be reviewed and used to inform the <u>seismic evaluation</u> walkdown-review and subsequent seismic capacity evaluations.

5.30.5.31. The detailed <u>seismic evaluation</u> walkdown should review all the selected SSCs to the extent feasible. The seismic <u>capability</u> engineers should assess the construction and seismic robustness of the SSC, its support structure, <u>and</u> anchorage, the potential consequences of credible sources of spatial and other seismic interactions that <u>maymight</u> affect it, and the potential <u>for</u>, and consequences of <u>a</u> a <u>seismic seismically</u> induced fire, flood, or spray resulting from the failure of the SSC. <u>ReviewFor the review</u> of SSCs in inaccessible or restricted access locations <u>may use</u>, available supplemental information <u>may be used</u> (see para. 5.32). For groups of similar SSCs, a detailed review may be conducted of a lead item<u>and</u>, followed by less detailed walkbys <u>may be conducted on of</u> the <u>remainingother</u> items to confirm <u>their</u> similarity and record any differences relevant to the <u>seismic</u> capacity evaluation. For SSC classes with an excessively large number of <u>often</u>-similar items (e.g. local instruments-<u>and</u>, passive elements), the walkbys may be performed on a sampling basis. For distribution systems, the walkdown may be performed on a sampling basis in areas of interest that. The areas of interest should be identified by thea systems engineer and should focus on identifying representative represent the as-built configurations for <u>seismic</u> capacity evaluations.

5.31.<u>5.32</u>. Post<u>The post</u>-walkdown activities should be performed to resolve include any actions that could not be performed in the field. These post-walkdown activities should be identified in the walkdown documentation. Examples of, such actions include as the review of photographs, construction records, and other documentation in lieu of field observation of for inaccessible

SSCs, SSC internals, SSC anchorage, or SSC seismic load <u>pathpaths</u> to the structure (e.g. obscured by a raised floor). <u>TheHowever, the</u> walkdown <u>determinationsfindings</u> should be <u>made</u>-based on field observations to the extent feasible. <u>These post-walkdown activities should</u> <u>be identified in the walkdown documentation.</u>

5.32.5.33. The seismic <u>evaluation</u> walkdown should be properly documented as an important product of the <u>seismic</u> safety evaluation. This The documentation should include the following:

- (a) Summary of the walkdown planning (see paras 5.29(a)—<u>5.29(d)</u>) and execution activities;
- (b) The final list of selected SSCs (including justification for SSCs removed or added based on the basis of the walkdown);
- Summary of the main walkdown findings and recommendations relevant to the seismic capacity evaluation for the selected SSCs;
- (d) Seismic evaluation data collected for all SSCs. This data is typically entered in template forms for each SSC class and should be populated inused to populate the SSC database (see para. 5.27(b)).

CONSIDERATIONS ON SEISMIC CAPABILITY OF NUCLEAR INSTALLATIONS FOR DEFENCE IN DEPTH LEVEL 4

5.33.5.34. The design and as-is conditions of the installation are required to provide adequate seismic margin to ($\frac{1}{10}$) protect items important to safety and avoid cliff edge effects; and ($\frac{1}{10}$) protect items ultimately necessary to prevent an early radioactive release, or a large radioactive release, in the case that levels of <u>if</u> natural hazards greater thanoccur at levels that exceed those considered for design occur: (see Requirement 17 of SSR-2/1 (Rev. 1) [3], Requirement 19 of SSR-3 [5], and Requirement 16 of SSR-4 [6].

5.34.<u>5.35</u>. Defence in Depth-Level 4 concerning seismic hazardof the defence in depth concept corresponds to the mitigation of severe accidents and prevention of large releases. The list of selected SSCs to be evaluated for adequate <u>seismic</u> margins should include items needed to perform mitigation functions associated with design extension conditions-[3]. For instance, the list should include the items for the protection of the containment system, (for <u>nuclear</u> installations with such a system, or for protection of the last confinement barrier against large releases, (for other <u>nuclear</u> installations.).

5.35.5.36. For the prevention of an early and/radioactive release or large releases radioactive release, the minimum seismic margin should be consistent with the containment or confinement seismic performance goal (e.g. a large <u>or</u> early release frequency of less than 10^{-6} per year for a new nuclear power reactor design, see SSG-67 yr⁻¹)-[9]).-

5.36.5.37. In seismic safety evaluation of adequate margins for items performing mitigation functions associated with design extension conditions-[3], uncertainty in the seismic margin estimates should be properly considered.

IMPLEMENTATION OF SEISMIC MARGIN ASSESSMENT FOR NUCLEAR INSTALLATIONS

5.37.5.38. The SMA methodology should comprise the following steps:

- (1) Selection of the assessmentevaluation team (see para. 5.15);
- (2) Selection of the reference level earthquake (see para. 5.5);
- (3) Plant familiarization and data collection (see Section 4);
- Selection of success path(s) (see paras 5.17(b) and 5.39) and <u>identification of the list of selected SSCs list</u> (see para. 5.18);
- (5) Systems walkdown (see para 5.21) and seismic Seismic evaluation walkdown (see para. 5.23); 5.19);
- (6) Determination of the seismic responses of SSCs for input to <u>seismic</u> capacity calculations;
- (7) Determination of HCLPF capacities for the selected SSCs and the installation;
- (8) <u>Specific Application of specific considerations for nuclear reactors; (see paras 5.48 and 5.49);</u>
- (9) Peer review (see Section 8);
- (10) DocumentationPreparation of documentation (see Section 8).

5.38.5.39. Specific guidance for the selection of The following recommendations should be taken into account in selecting the success path(s) and selected SSCs infor the SMA methodology should include the following:

(a) Multiple alternate success paths may be selected that include availableto ensure diversity and redundancy in the front-line and support systems. In some Member States,



<u>the</u> selection of at least two success paths for some installations is required by the regulatory body.

- (b) The systems engineers should formulate the candidate success path(s) to reach an acceptable end state (see para. $5.16)^{43}$, with input from operations operating personnel. AlternativeDifferent paths should comprise differinginclude different operational sequences and SSCs to the extent possible.
- (c) If multiple success paths are selected, one should be designated as the primary-success path. The primary success path should be the path for which it is judged easiest to demonstrate a high seismic safety margin-thereto, and should be consistent with the plant design manuals, operational procedures and trainingemergency response procedures.
- (d) The seismic <u>capability</u> engineers should support the determination and prioritization of success paths by qualitative assessment of ruggedness and seismic vulnerability of the selected SSCs based on knowledge ofgained from the systems walkdown and previous seismic<u>safety</u> evaluations.
- (e) Non-seismic failures of SSCs and system outages (e.g. random or maintenance-related) failures of SSCs and system outages should be reviewed. Candidate The use of success paths should avoid relying that rely on SSCs with high random failure rates should be avoided to the extent possible.
- (f) The actions required of the operations staffActions to be taken by operating personnel should be reviewed and assessed givenin the light of the common cause nature of the earthquake. CandidateThe use of success paths should avoid relyingthat rely on operator actions that cannot be executed with high confidence given their (e.g. owing to the timing, durations, installation or duration of the action, operational and emergency procedures and training, andat the installation, or the potential for confusionincreased stress levels for personnel or interference with their other responsibilities) should be avoided.

Determination of seismic responses

⁴³ For <u>water cooled</u> nuclear reactors, the <u>fundamental safety</u> function <u>"of heat</u> removal <u>of heat</u> from the reactor..." (see <u>Requirement 4 of SSR-2/1 (Rev. 1) [3]</u>) to achieve an acceptable end state, as described in para. 5.16, involves control of the reactor coolant pressure, control of the reactor coolant inventory, and decay heat removal.

5.39.5.40. The seismic responses of buildings and other structures on the <u>list of selected SSCs</u> list should be determined for use in the generation of seismic input motions for <u>the SSCs</u> supported by each structure. These <u>seismic responses</u> may also be <u>requiredneeded</u> for the seismic capacity evaluation of the structure if its failure modes of interest (see appendix) cannot be qualitatively screened out as <u>relativelyseismically</u> rugged in accordance with para. 5.22. The seismic responses of systems and components should be determined for their seismic capacity evaluations.

5.40.5.41. The <u>SSCseismic</u> responses <u>of SSCs</u> to the reference level earthquake should be determined with a high confidence level (<u>see e.g. Paragraphsection</u> 5.1.2.6 of Ref. [11]). <u>Probabilistic</u>. Determination of seismic responses may use probabilistic or deterministic methods of structure analysis- may be used to determine seismic responses. Probabilistic methods of analysis use best estimate-centred parameter values and include explicit treatment of uncertainties. Acceptable deterministic <u>analysis</u>-methods should include conservative provisions to account for the effect of uncertainties (e.g. <u>dueowing</u> to analytical procedures and parameter values) and the sources of randomness associated with the reference level <u>earthquake</u> ground motions⁴⁴ that were not included in the seismic hazard analysis.

5.41.5.42. Determination of The following recommendations should be taken into account in determining seismic responses for buildings and other structures should consider the following recommendations:

- (a) NewCurrent mathematical models of the structure should be used for the new seismic response analysis for the reference level earthquake ground motions-using-current mathematical models of the structure is recommended. Scaling. The scaling of previous seismic response analysis results (e.g. design-basis analyses) based on the ratios of reference-level to design-basis earthquake ground motions may be justifiable. Scaling is most considered appropriate for rock sites where the design-basis models of the structures are considered linear -and- median centred, and where the spectral shapes of the design basis and reference level earthquakes are sufficiently similar.
- (b) For vibratory ground motion input, response spectrum analysis methods may be sufficient for structures without significant soil-_structure-_interaction (SSI)-effects. <u>ResponseFor structures with significant soil-structure interaction effects, response</u>

⁴⁴ For reference, modern PSHAs <u>Modern probabilistic seismic hazard analyses</u> incorporate most sources of ground motion randomness. One common exception is randomness due to earthquake component-to-component variability. 64

history methods (also called sometimes referred to as 'time history methodsmethods') should be used otherwise. Equivalent linear or explicitly nonlinear methods may be used as appropriate for the expected responses.

(c) For non-vibratory ground motion input (e.g. response to liquefaction settlement or slope deformation), quasi-static analysis methods should typically be sufficient.

5.42.5.43. Determination of The following recommendations should be taken into account in determining seismic responses for systems and components should consider the following recommendations:

- (a) The seismic responses may be determined <u>using either by a</u> new analysis of the response to seismic input motions at the system or component supports resulting from the reference level earthquake ground motions<u>or</u>, by the scaling of previous response analysis results <u>based</u> on the <u>basis of the ratios of the seismic input motions to the system</u> <u>or component/system</u>, or <u>by</u> physical testing.
- (b) For vibratory ground motion input, analysis of the system or component or system response may be performedanalysed as coupled or uncoupled with the supporting structure model. Coupled response analysis should be used if significant dynamic interaction effects are expected.
- (c) For non-vibratory ground motion input, quasi-static analysis methods should typically be sufficient.

Determination of HCLPF capacities for the selected SSCs and the nuclear installation

5.43.5.44. The seismic capacities of the selected SSCs should be characterized <u>usingby</u> determining their HCLPF capacities. The HCLPF capacity⁴⁵ of an SSC is expressed <u>as a</u> function of the hazard parameter (PGApeak ground acceleration or spectral acceleration) corresponding to the scale factor⁴⁶ on the reference level earthquake ground motions at which there is at least 95% confidence of a <u>less than</u> 5% probability of failure. <u>ItAlternatively, the</u>

⁴⁵—Determining HCLPF capacities <u>can and isfor SMAs are</u> often <u>performeddetermined</u> using deterministic <u>evaluationanalysis</u> methods similar to following design code procedures (e.g., the conservative deterministic failure margin method) in lieu of explicit propagation of uncertainties in the seismic capacity evaluation. <u>Alternatively, HCLPF capacities</u> may be determined explicitly using probabilistic fragility analysis methods such as the separation of variables. The latter methods are used infrequently for SMAs compared to SPSAs.

⁴⁶ The scale factor is to be multiplied by the PGApeak ground acceleration or Spectral Accelerationspectral acceleration of the RLE, in orderreference level earthquake to get the HCLPF.

HCLPF capacity may alternatively be represented by an earthquake motion levelhazard parameter at which the expected (mean) probability of failure is 1% or lower.47

5.44.5.45. The determination of HCLPF capacities should be performed determined by the seismic capability engineers. More detailed seismic capacity evaluations should be performed for the SSCs with a relatively low HCLPF capacity that are requiredneeded in each success path. More simplified conservative, bounding-case, or screening-based capacity evaluations may be performed for other SSCs in each success path without affecting the success pathpath's HCLPF capacity.

5.45.5.46. The HCLPF capacity of a success path should be taken as equal to the HCLPF capacity for the SSC with the lowest HCLPF capacity in the path. More than one independent success pathspath should be considered. The installation-level HCLPF capacity mayshould be taken as equal to that of the success path with the highest HCLPF capacity.

5.46.5.47. The reference level earthquake, and the HCLPF capacities for the installation-level and SSC HCLPF capacitiesSSCs should be reported. The weak link(s) in each success path should be identified for consideration of potential improvements or other actions (see Section 7).

Considerations for nuclear power plants

5.47.5.48. Seismic The seismic margins of the containment and confinement systems for nuclear power plants should be determined. Items Features such as penetrations, and equipment and personnel hatches, and considerations such as impact between structures, and containment performance under elevated temperature and pressure caused by core damage should be reviewed. Credible potential seismic weak links in the containment and confinement systems should be explicitly included in the success path HCLPF capacity determination. Alternatively, Level 2 probabilistic safety assessment for internal initiating events (see IAEA Safety Standards Series No. SSG-4, Development and Application of Level 2 Probabilistic Safety Assessment for Nuclear Power Plants [21] may be performed to evaluate containment response to beyond design basis events.

5.48.5.49. A detailed walkdown inside the containment to verify that all small lines in a nuclear power plant can withstand the reference level earthquake is resource-intensive and possibly

⁴⁷ The HCLPF capacity is exactly equal to the value of this parameter when the standard deviation terms for randomness and uncertainty are equal. 66



impractical <u>dueowing</u> to (<u>ia</u>) the radiation exposure hazard to the walkdown team, and (<u>iib</u>) the challenges of an exhaustive review of potential seismic spatial interactions affecting small lines in a crowded space. As a practical alternative, <u>the-SMA</u> may be performed by ensuring that any success path is capable of sustaining concurrently the loss of <u>offsiteoff-site</u> power and a small loss of coolant accident inside the containment. <u>Alternatively, the integrity of small bore lines</u> could be verified on a sampling basis.

PSA-IMPLEMENTATION OF PROBABILISTIC SAFETY ASSESSMENT BASED SEISMIC MARGIN ASSESSMENT FOR NUCLEAR INSTALLATIONS

5.49.5.50. The PSA-based SMA methodology should comprise most of the same steps $\frac{1}{1000}$ of $\frac{1}{1000}$ should comprise most of the same steps $\frac{1}{1000}$ should be same steps $\frac{1}{1000}$ should be should be

- (a) The selection of success path(s) (Stepstep 4) isshould be replaced by the accident sequence event tree and fault tree analysis;
- (b) The identification of the <u>list of selected SSCs list (Step(step</u> 4) <u>isshould be</u> based on the requirements of the accident sequence analysis;
- (c) <u>Determination of The HCLPF equacity capacities</u> for the installation (<u>Stepstep</u> 7) is <u>performed</u>should be determined differently-(see para. 5.54);
- (d) Enhancements of PSA-Based SMA may include Human Errorserrors and Non-Seismic Random Failures non-seismic random failures should be included.

5.50.<u>5.51</u>. <u>Development of the The</u> accident sequence event trees and fault <u>treestree</u> logic <u>modelmodels</u> should be <u>performeddeveloped</u> following the SPSA methodology (see paras 5.56 and _5.57).

5.51.5.52. The list of selected SSCs list should be identified in a similar to the selected SSCs listway as for the fragility evaluation in the SPSA methodology (see para. 5.58).

5.52.5.3. Determination of the The HCLPF capacities for the selected SSCs is are typically performeddetermined in a similar way to theas for SMA-method. Depending on the desired end-product of the safety assessment, the following refinements should be considered:

 (a) Development of conservatively biased seismic fragility estimates for the SSCs. This can be <u>performed_achieved</u> by assigning a generic or estimated value of the variability to define a lognormal function anchored to <u>be combined with</u> the HCLPF capacity at 1% mean probability of failure⁴⁸-to estimate a fragility function.⁴⁹

(b) Development of detailed seismic fragilities (i.e.in a similar toway as for the SPSA method — see para. 5.62) for SSCs that are identified to govern the installation-level HCLPF capacity.

5.53.5.54. The installation-level HCLPF capacity should be determined by incorporating all minimal <u>eut-setscutsets</u> that can lead to <u>an-unacceptable</u> end <u>state. Itstates. The capacity</u> may be computed <u>followingusing</u> one of the following two approaches:

- (a) The 'min-max' approach: Each <u>cut-set-HCLPF</u> capacity <u>may be in the cutset is</u> taken <u>as</u> equal to <u>that of</u> the HCLPF capacity <u>for theof</u> SSC with the highest HCLPF capacity in the <u>cut-set⁵⁰ cutset</u>. The installation-level HCLPF capacity <u>should be staken as equal to</u> the lowest <u>cut-set-HCLPF</u> capacity-<u>in the cutset.⁵¹</u>
- (b) The explicit quantification approach: An estimated fragility curve <u>may befor each cutset</u> <u>is</u> derived <u>for each cut set</u> from the seismic fragilities (and non-seismic failure probabilities) of the <u>cut setcutset</u> components using a Boolean AND gate. An estimated fragility curve for the installation <u>may beis</u> derived from the <u>cut setcutset</u> fragilities using a Boolean OR gate. The installation_level HCLPF capacity <u>may beis</u> computed by identifying the 1% mean probability of failure point on the latter fragility curve.

5.54.<u>5.55.</u> The reference level earthquake, and the installation-level and all significant cut-setcutset HCLPF capacities should be reported. The weak-_link cut setscutsets, the corresponding accident sequences, and the failure modes and HCLPF capacities of SSCs leading to these accident sequences should be identified for consideration of potential improvements or other actions (see Section 7). Estimated fragility curves for the installation and the weak-_link cut setscutsets, if developed, should also be reported.

⁴⁸-In this case, an estimate of the variability biased low is conservative, since the fragility curve is anchored to a low apacity value, the 1% point.

 ⁴⁹ In this case, an estimate of the variability biased low is conservative, since the fragility curve is anchored to a low probability of failure value, that is the HCLPF capacity point.
 ⁵⁹ The min-max approach produces estimates that are more approximate than the explicit quantification approach.

⁵¹ The min-max approach produces estimates that are more approximate than the explicit quantification approach.

⁶⁸

IMPLEMENTATION OF SEISMIC PROBABILISTIC SAFETY ASSESSMENT FOR NUCLEAR INSTALLATIONS

5.55.5.5.5. The SPSA methodology comprises hould comprise most of the same steps of as the SMA methodology (see para. 5.38), with the following modifications:

- (a) Step 4 should be replaced by the development of the accident sequence event tree and fault tree logic model and the identification of the <u>list of selected SSCs-list accordingly</u>;
- (b) Human reliability analysis for operator actions in the context of a seismic event should be added;
- (c) Step 7 should be replaced by seismic fragility evaluation of the SSCs and seismic risk quantification for the nuclear installation.

5.56.5.57. The accident sequence logic model should include the analysis of potential seismically induced initiating events, and installation response considering the impact of the seismic event on SSCs, and operator actions. For example, the The most popular common approach taken in the Member States is to use seismic event trees to model accident sequences, and fault trees to model basic seismie failure events ⁵², (see Ref. [10] for a more detailed description). If the nuclear installation has an existing internal events PSA probabilistic safety assessment logic model, which is typically a regulatory requirement for nuclear power plants, the seismic accident sequence logic model should be developed by modifying the internal events logic model to account for seismic seismically induced failures and initiating events that are not included in the internal events PSA. For example probabilistic safety assessment. The following considerations should be taken into account:

- (a) The common cause nature of seismic events imposes concurrent demands on the SSCs in the installation and on surrounding infrastructure and may lead to simultaneous failures whose correlation should be considered in the logic model.
- (b) The range of seismic ground motions represented by the seismic hazard curve range from moderate to very large earthquakes. The resulting probabilistic distributions of seismic demands at the plant level <u>ledlead</u> to distribution of the core <u>and/or fuel</u> damage frequency, <u>of the large or early release frequency, or of</u> other risk metrics of interest, <u>as</u> <u>a</u> function of the hazard parameter.

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52 Ref. [10] provides a more detailed description

- (c) Earthquakes might cause initiating events not applicable to internal events PSAprobabilistic safety assessment.
- (d) Earthquakes might cause failures of passive SSCs such as structures and distribution systems that are not included in the internal events <u>PSAprobabilistic safety assessment</u>.
- (e) Earthquakes might result in seismic interaction failures (e.g. seismic-seismically induced fire).
- (f) SPSA accident sequence logic should include both potential seismic and <u>potential</u> nonseismic (e.g. random) SSC failures within the time <u>requiredtaken</u> to reach an acceptable end state.

5.57.5.58. The system logic model⁵³, either new or modified from an existing internal events PSAprobabilistic safety assessment logic model, should include all credited systems that are relied upon to prevent the progression of accidents due to seismic-seismically induced initiating events to an unacceptable end state (see DS523 [15]).- Existing accident sequence models (e.g. event trees) should be modified or supplemented by new ones unique to the SPSA (e.g. failure of major structures that lead directly to unacceptable end states). SystemExisting system reliability models (e.g. fault trees) should be modified to include all credible seismic-seismically induced and non-seismic failure modes and to include_a as applicable, credited recovery actions (e.g. operator intervention-and, mitigation systems). Common-cause failures and fragility correlations between basic events should be modelled.

5.58.5.59. The list of selected SSCs list for the seismic evaluation walkdownSPSA should include all the SSCseach SSC whose seismic-seismically induced failures contributefailure contributes to the basic events in the accident sequence logic model. This list typically includes significantly more SSCs than are needed for the SMA methodology, which only involves includingneeds enough SSCs sufficient to achieve a limited number of success paths. The selected SSCs list forFor the fragility evaluation-, the list of selected SSCs should be shortened by excluding the SSCs screened out as described in para. 5.22 and, by assigning them nominally high or low fragilities.

5.59.5.60. Determination The determination of seismic responses of SSCs should generally be consistent with the recommendations provided for SMA in paras 5.40–5.43. However, infor the SPSA methodology, the probability distributions of the seismic responses should be

 53 For nuclear power plants, this system logic model is commonly referred to as <u>a</u> 'seismic plant response model'. 70 characterized in addition to generating the generation of high_confidence conservative response estimates for HCLPF computations, the probability distributions of the seismic responses should be characterized. This characterization should be performed by using median-centred values and associated variabilities of the input parameters (e.g. material properties) and analytical models consistent with the reference <u>level</u> earthquake ground motion level.

5.60.5.61. Fragility curves should be developed for items on the <u>list of</u> selected SSCs-list. A fragility curve should characterize the probability of failure of an SSC conditioned on an earthquake loading intensity parameter. The SSC failure mode(s) evaluated for each SSC should be causally related to the basic events in the system logic model. Earthquake intensity is typically characterized by a ground motion parameter (e.g. <u>PGA</u>) and <u>peak ground</u> acceleration) but may alternatively be characterized by a local parameter (e.g. in-structure acceleration). The variability represented by each fragility curve should include the effects of inherent randomness and epistemic uncertainty on the corresponding SSC conditional probability of failure.

5.61.5.62. Seismic fragility evaluations should be performed at a level of rigour appropriate forto the risk significance of the SSC. The following three approaches represent an ascending level of rigour:

- (1) Generic fragility curves may be used for SSCs with <u>a</u> negligible contribution to seismic risk. These may include nominally low and nominally high generic fragilities for SSCs screened <u>out</u> in accordance with para. 5.22, and database-based (i.e. not componentandor installation-specific) fragilities for other SSCs that meet certain inclusion rules.⁵⁴.
- (2) HCLPF capacity-_based fragilities may be developed as described in para. 5.53(a). These fragilities should be sufficiently component- and installation-specific to be used for significant risk contributors. The use of these fragilities is not recommended for dominant risk contributors.
- (3) Detailed fragilities <u>incorporating expected SSC-seismic responses and capacities of SSCs</u> and explicit treatment of variability <u>dueowing</u> to uncertainty and randomness <u>may be developed and used for risk-significant SSCs</u>. The use of these fragilities is recommended for dominant risk contributors.

⁵⁴ The SSCs assigned generic fragilities should be confirmed in the final risk quantification to have no significant risk contributions, which may require might necessitate refinement iterations.

5.62.5.63. Assessment of humanHuman failure event probabilities should be performed consideringassessed taking into consideration that the unique challenges of earthquakes and the level of damage, confusion they cause, increased stress levels, concurrent genuine and spurious failure alarms, and the potential loss of indicator signals on shapingmight shape human performance. More guidancerecommendations on human reliability modelling can be foundare provided in DS523 [15] and further information is provided Ref. [21].[22].

5.63.5.64. Risk quantification should be performed by combining the SSC fragilities, minimal cut-setcutset Boolean mathequations, and seismic hazard curves over an earthquake intensity parameter range of interest. The installation-level fragility curve should be computed explicitly at each intensity level from the SSC fragilities, non-seismic failure rates, and human failure probabilities, in accordance with the approach described in para. 5.54(b) (except using the full fragility curve instead of the min-max approach or estimated curves). This fragility curve should be integrated with the earthquake severity occurrence rates according to the hazard curve to compute the annual frequency of unacceptable performance. Depending on the safety evaluation objectives and regulatory requirements, this annual probability may be determined as a point estimate of the mean value or as a probability distribution.

5.64.5.65. The following SPSA outcomes should be reported:

- (a) The frequencies of unacceptable end states (e.g. core damage, large <u>or early radioactive</u> release);
- (b) Description of the major seismic-seismically induced initiating events and of the safety functions and/or mitigation functions included in the system logic model;
- (c) Lists of seismic fragilities and non-seismic failure rates developed for all SSCs, and of human error probabilities developed for operator actions;
- (d) Identification of the risk-_significant accident sequences, seismic-seismically_induced failures and associated SSCs, non-seismic failures, and operator actions, to allowfacilitate understanding of the likely accident scenarios and consideration of potential improvements or other actions (see Section 7);
- Identification of the installation-level fragility curve, the range of earthquake intensity that <u>contributecontributes</u> most significantly to seismic risk, and any potential cliff edge effects;
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- (f) If applicable, identification of safety-related SSCs whose contribution to seismic risk is negligible for potential consideration in risk informed design decisions (see Section 7);
- (g) Assessment of the sensitivity of the results to major modelling assumptions;
- (h) Uncertainty ranges of annual frequencies and identification of their major contributors.

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6. EVALUATION OF SEISMIC SAFETY FOR <u>NUCLEAR</u> INSTALLATIONS OTHER THAN NUCLEAR POWER PLANTS

6.1. This section provides guidance on the seismic safety evaluation of a broad range of nuclear installations (see para. 1.1+10) other than nuclear power plants.

6.2. <u>SeismieThe seismic</u> safety evaluation of nuclear installations other than nuclear power plants should be based on <u>a graded approach</u>, as recommended in the following paragraphs. The intent is thatpurpose of the evaluation verifies to verify that the performance of the SSCs important to safety within the installation is acceptableare still able to fulfil their safety functions in the event of an earthquake.

6.3. The methodology to be followed <u>infor</u> evaluating nuclear installations other than <u>nuclear</u> power plants is essentially identical to that for nuclear power plants; however, the end state will be unique for each installation. In the case of a nuclear power plant the end state <u>most commonto</u> <u>be achieved</u> is <u>typically</u> to prevent core damage (i.e. <u>to</u> safely shut down the <u>plantreactor</u> and remove residual heat from irradiated fuel) and to prevent a -large <u>or</u> early <u>radioactive</u> release. For nuclear installations other than nuclear power plants, <u>thean example</u> end state <u>to be achieved</u> may be to prevent <u>the</u> leakage of aerosolized contaminants, <u>for instance, in the case of from</u> a fuel processing facility. Once the desired end state is <u>establisheddefined</u>, the methodology for assessing the <u>installation's</u> ability to achieve this end state should be <u>evaluated using</u> <u>theselected</u>: SPSA, PSA-_based SMA₇ or SMA-<u>approaches</u> presented in Sections 3 and 5 of this Safety Guide.

HAZARD CATEGORY OF A NUCLEAR INSTALLATION

6.4. For the purpose of seismic safety evaluation, each SSC that is required to performperforms a seismic risk mitigating function should be assigned to a seismic design elass (SDC), category, which is a hierarchical category that denotes its importance in mitigating seismic hazard (see Section 93 of DS490SSG-67 [9]). The seismic design elasscategory assigned to the SSC is a function of the severity of adverse radiological and toxicological effects — on workers, the public; or the environment — of the hazards that might result from the

seismic failure of the SSC⁵⁵, ⁵⁶ A framework like the one given in the Annex to this Safety Guide or in Table 2 of SSG-67 [9] should be used in establishing the seismic design category for the SSCs of the nuclear installation. Additionally, Table A–1 in the annexAnnex to this Safety Guide provides an example of criteria for use in determining the seismic design class. A framework like the one given in the annex of this Safety Guide or in Table 2 of DS490 [13] should be used in establishing the seismic design class for the SSCs of the nuclear installationcategory.

6.5. A similar approach should be used to categorize a nuclear installation into a hazard category, as a function of the risk to <u>workers</u>, the public, workers, or the environment from a potential unmitigated radioactive release from the installation (see Section 9 of DS490. [13]). AnSSG-9 (Rev.1).[7]). Table A–1 in the Annex to this Safety Guide provides an example of possible nuclear installation-hazard categories (high, moderate and low) is also provided in Table A–1.).

6.6. A conservative screening process should be used prior toundertaken before categorizing a nuclear installation. In this process, it is assumed that the complete radioactive inventory of the installation is would be released by a seismically initiated accident. If this process, the public, or the environment, and no other specific requirements are imposed by the regulatory body for such an the nuclear installation in question, the installation may be screened out from the seismic safety evaluation. For equipment or tanks that need to be operated and/or maintained in controlled atmosphereconditions (e.g. inert glove boxes, high level waste storage tanks), the possible consequences (e.g. fire and/or, explosion) of the failure of the controlled conditions should be considered in the screening process. If, even after such screening, some level of seismic safety evaluation is needed, national seismic codes for industrial facilities may be used.

6.7. If the results of the screening process show that the consequences of the unmitigated releases arewould be unacceptable, a seismic safety evaluation of the <u>nuclear</u> installation should be carried outperformed. For this purpose, the seismic hazard at the site should be determined,

⁵⁵ For example, in the United States of America, nuclear installations are assigned to seismic design classes (see appendix). SSCs that perform a safety function are placed into a design category based on the unmitigated consequences that may result from the failure of the SSC by itself or in combination with other SSCs. Consideration is given to consequences to the worker, the public, or the environment.

⁵⁶ For example, in the United States of America, SSCs that perform a safety function are placed into a seismic design category, referred to as a 'seismic design class' based on the unmitigated consequences that might result from the failure of the SSC by itself or in combination with other SSCs (see Annex). Consideration is given to consequences to workers, the public or the environment.

in accordance with the recommendations provided in paras 2.19-2.25. The seismic input for the safety evaluations should not be less than a peak ground acceleration of 0.1 g at the <u>free</u> <u>field or</u> foundation level.

SELECTION OF PERFORMANCE TARGETS FOR EVALUATION OF SEISMIC SAFETY FOR INSTALLATIONS OTHER THAN NUCLEAR POWER PLANTS

6.8. A 'performance target',target — expressed as a mean annual frequency of failure due to the earthquake hazard, — should be assigned to each of the seismic design <u>classes_categories</u> described in para. 6.4. The performance targets represent the acceptable calculated mean annual frequency of <u>seismic_seismically</u> induced failure of SSCs within a seismic design <u>class_category</u> (See Section <u>93</u> of <u>DS490SSG-67</u> [9]). The failure of an SSC is associated with a particular failure mode and a limit state⁵⁷. Table A–2 in the <u>annex_Annex</u> to this Safety Guide provides an example of performance targets selected for different seismic design <u>classes_categories</u>.

6.9. A performance target should also be defined for the nuclear installation, as the maximum mean annual frequency of unacceptable performance of the installation due to the earthquake hazard (e.g. occurrence of unacceptable radioactive releases).

6.10. The overall performance of the <u>nuclear</u> installation (<u>i.e. the</u> annual frequency of failure) is the result of convolving the seismic hazard (hazard curves) with the installation-_level fragility (conditional probability of unacceptable installation behaviour, for each level of earthquake severity). The installation-_level fragility results from the seismic capacities of the SSCs and it can be obtained from <u>themthe SSCs</u> using <u>simplifiedsimple</u> or more rigorous methods.⁵⁸. Therefore, appropriately defined seismic design <u>classescategories</u> and performance targets for the SSCs within the installation should <u>lead to meetingallow</u> the performance target selected for the nuclear installation as a whole to be met.

6.11. ThereAccording to para 7.4 of SSG-67 [8], there is a correlation between the hazard level used for design, the seismic margin achieved by the design and the installation level seismic performance goal, as described in Section 7 of DS490 [13], In this context, the

⁵⁷ A 'limit state' is the limiting acceptable condition of the SSC, so that <u>for which</u> its intended safety function is kept. For example, the failure limit state for a column that is supporting a safety class pressure vessel would bethe limit state at which the <u>loss of column loses its</u> load carrying capacity through either buckling or collapse. For a mechanical pump with a safety function that requires operability, the <u>failure limit state would beat which</u> the <u>loss of pump loses its</u> operability.

⁵⁸ Those The various methods of obtaining installation-level fragility are discussed described in Section 5. In deterministic SMA, (the simplest method₂), it is usually assumed that the installation-level fragility can be derived just from the seismic capacity of the weakest SSC required needed to bring the installation to a safe state and keep it in a safe state during a specified period of time.

minimum requirednecessary seismic margin of the nuclear installation is related to the seismic design basis and the target <u>seismic</u> performance goal of the installation. <u>Seismie</u>: the seismic margin in this context can be regarded<u>considered</u> as a surrogate for the installation levelseismic performance goal. The basis for the graded approach is described in paras 6.12 and 6.13.

GRADED APPROACH FOR ACHIEVING SELECTED PERFORMANCE TARGETS IN THE EVALUATION OF SEISMIC SAFETY FOR EVALUATION OF NUCLEAR INSTALLATIONS

6.12. A graded approach should be used for demonstrating that nuclear installations meet the performance targets (see para. 6.9) assigned to them. The level of rigour applied in the <u>seismic</u> safety evaluations should range from simple, <u>(for low hazard installations,</u>) to complex, <u>(for high hazard installations,</u>), as follows:

- (a) For low hazard installations, the seismic capacity evaluation methods for the selected SSCs may be based on <u>simplifiedsimple</u> but conservative static or equivalent static procedures, similar to those used for industrial hazardous facilities, in accordance with national practice and standards. Similarly, the seismic hazard to be used in these evaluations may be taken from national building codes and <u>mapseismic hazard maps</u> and does not need to be taken from a site-specific <u>PSHA.probabilistic seismic hazard</u> <u>analysis</u>. If a <u>PSHAprobabilistic seismic hazard analysis</u> exists, however, the seismic hazard from that study may be used.
- (b) For selected SSCs of installations in the moderate hazard category, the seismic safety evaluation should typically be performed using the methodologies described in Section 5, but the corresponding performance target is set lower than for installations in the high hazard category (see <u>annexAnnex</u>). Either the SMA-or, SPSA or PSA-based SMA approach may be used <u>depending on the objective and scope of the seismic safety evaluation</u>.
- (c) For selected SSCs of installations in the <u>higherhigh</u> hazard category, methodologies for seismic safety evaluation as described in Section 5 should be used (i.e. no application of a graded approach).

6.13. In a particular SSC, the performance target associated with a failure mode should be demonstrated by one of the following methods:



- (a) Showing compliance with a design code that was developed withusing a reliabilitybased approach⁵⁹. The design levelbasis earthquake should be selected based on the basis of an annual frequency of exceedance that is consistent with the performance target for the particular SSC.
- (b) Showing adequate seismic margin beyond a site specific reference level earthquake. The reference level earthquake should be selected based on an annual frequency of exceedance that is consistent with the performance target for the particular SSC.
- (c) Explicit computation of Explicitly computing the annual frequency of failure, using a SPSA. In the SPSA this case, it is very important to use the ground motion from a site specific PSHAprobabilistic seismic hazard analysis, and to ensure that the SSCs important to safety have been properly categorized and the appropriate limit states have been defined.

⁵⁹ <u>"Reliability-In a 'reliability</u> based approach'<u>refers to an approach in which, the</u> design code requirements are intended to achieve a predefined maximum probability of failure for a given set of loadings or external actions.

7. USE OF SEISMIC SAFETY EVALUATION RESULTS FOR NUCLEAR INSTALLATIONS

POST-EARTHQUAKE ACTIONS BASED ON THE SEISMIC SAFETY EVALUATION OF NUCLEAR INSTALLATIONS

7.1. The<u>In</u> the nuclear installationinstallation's post-earthquake procedures, including emergency plans, procedures for post-earthquake inspections, and plans for re-start, should considerrestart, the lessons learned in the seismic safety evaluation, should be taken into consideration. As a result of the seismic safety evaluation, the facility owneroperating organization and the regulatory body will have a better understanding of those SSCs that are important to seismic safety. They will also have a better understanding of any seismic weak links associated with the nuclear installation. All this information should be taken into account in the definition of post-earthquake actions.

RISK-_INFORMED DECISIONS BASED ON THE SEISMIC SAFETY EVALUATION OF NUCLEAR INSTALLATIONS

7.2. The<u>A</u> programme for <u>the</u> seismic safety evaluation of an existing nuclear installation may <u>result ininclude identification of</u> a subset of the selected SSCs that do not meet the established acceptance criteria. If that is the In this case, then consideration should be given to <u>physicaltechnical</u> upgrades or strengthening programmes. The<u>When making a</u> decision about implementing this kind of programme should considerwhether to implement upgrades or strengthening programmes, the potential seismic risk reduction versus should be weighed against the implementation costs, and time, taking into consideration the time at risk concept, consideringlength of the remaining lifeoperating lifetime of the installation.

7.3. In many instances there are <u>alternatealternative</u> solutions for reducing the <u>potential</u> <u>seismic</u> risk to an appropriate level. These may include, for instance, such as the following:

- Reducing the <u>inventory of material</u> at risk to moderate or low <u>inventory</u> levels, <u>such so</u> that less demanding performance targets can be met;
- Upgrading the facility by strengthening <u>Strengthening</u> the SSCs that limit thea nuclear installation to <u>meetin meeting</u> the minimum seismic margin or are significant risk contributors;
- (c) Hardening the primary containment <u>suchso</u> that the <u>inventory of material at risk</u> for which the <u>'unmitigated radioactive release'release</u> amount was calculated is reduced.

Regardless of the option taken, sufficient diligence-the associated risk reduction should be exercised to be able to quantitatively calculate the reduction in risk associated with the option.be quantitively calculated. This risk reduction will come in the form of an increase in the computed margin if a seismic margins assessment method the SMA methodology was used, or in the form of a decrease in the annual frequency of failure of the selected SSCs if athe SPSA methodmethodology was used.

7.4. The cost associated with each of the alternate solutionsoption should also be quantified. 7.5.7.4. The <u>A</u> risk-_informed decision should look at the alternate solutions and consider<u>take</u> into account both the cost and the <u>potential seismic</u> risk reduction- of each option. Options that are easy to implement and for which there is very little<u>have</u> an appropriate cost involved should be implemented.given preference. For options that are very costly and for which there is involve very little risk reduction, the operating organization of the nuclear installation should work with the regulatory body to determine if the costs exceed<u>whether</u> the benefits from<u>are sufficient to</u> outweigh the small amount of risk reductioncosts.

DESIGN OF MODIFICATIONS IN EXISTING NUCLEAR INSTALLATIONS BASED ON THE SEISMIC SAFETY EVALUATION

7.6.7.5. Modifications In accordance with SSR-2/1 (Rev. 1) [3], SSR-3 [5] and SSR-4 [6], modifications to nuclear installations are required to be designed in accordance with recognized codes and standards and, at a minimum, to the original design standards. Design The design of upgrades needs to should meet the design criteria and performance targets appropriate forto the hazard category of the nuclear installation. Potential new seismic interactions introduced by new or modified SSCs should be assessed and eliminated to the extent practicable. More considerations for upgradingrelating to upgrades are provided presented in Ref. [10].

7.7.7.6. For the design of modifications, the seismic demand and the acceptance criteria should be established in compliance with the requirements of the regulatory body. The design for When designing seismic upgrades should consider, the available space and the working environment (e.g. radiation exposure).) should be taken into consideration. Upgrade concepts should (i) accommodate the existing configuration, to the extent possible, and (ii) should observe seismic interactions based on identified in the field inspection.

7.8.7.7. The type of upgrading of upgrade selected for existing structures or substructures depends on the additional seismic capacity that is needed. As a consequence, the <u>The</u> effects of the <u>upgradesupgrade</u> on interconnected systems and components (e.g. distribution systems)

should be evaluated, to verify that the upgrade enhances, rather than degrades, the overall seismic safety of the facility. Once the design of the finalselected upgrade is completed, the need for a dynamic analysis to generate new in-structure response spectra and displacements should be evaluated.

7.9.7.8. The type of <u>upgrading of upgrade selected for</u> existing systems and components <u>also</u> depends on the additional seismic capacity <u>that is</u> needed. Generally, the following types of <u>upgradingsystem and component upgrade</u> should be considered:

- (a) <u>UpgradingUpgrade</u> of anchorage, both for equipment and for supports in distribution systems;
- (b) Provision of additional lateral restraint, for distribution systems;
- (c) UpgradingUpgrade of electromechanical relays, to models with larger seismic capacity;
- (d) UpgradingUpgrade of critical components, to models with larger seismic capacity.

7.10.7.9. An important consideration is When selecting an upgrade design, priority should be given to prioritize the upgrades based on contribution options that contribute relatively more to the risk reduction of the installation on and upgrades that cost-benefit basis less to implement.

CHANGES IN PROCEDURES BASED ON THE SEISMIC SAFETY EVALUATION OF NUCLEAR INSTALLATIONS

7.11.7.10. Existing procedures for the inspection and maintenance of SSCs important to safety should be reviewed to ensure that the seismic capacity in the critical limit state for any SSC is not jeopardized as a part of normal operations (e.g. provisionplacement of scaffolding or temporary access items that maynight seismically interact with items important to safety).

8. MANAGEMENT SYSTEM FOR SEISMIC SAFETY EVALUATION FOR OF NUCLEAR INSTALLATIONS

APPLICATION OF THE MANAGEMENT SYSTEM TO SEISMIC SAFETY EVALUATION FOR OF NUCLEAR INSTALLATIONS

8.1. The management systems In accordance with para. 4.8 of IAEA Safety Standards Series No. GSR Part 2, Leadership and Management for each of the organizations involved in the seismic safety evaluation Safety [23], a management system for a nuclear installation is required to be developed, applied and continuously improved. The management system should be established and implemented before the start of the seismic safety evaluation programme [22] [23], begins (see also IAEA Safety Standards Series No. GS-G-3.1, Application of the Management System for Facilities and Activities [24]). The management system is required toshould cover all processes and activities of the seismic safety evaluation, in particular, including those relating to data collection and data processing, field and laboratory investigations, and the analyses and evaluations that are within the scope of described in this Safety Guide. It is The management system should also required to cover those processes and activities corresponding to the upgrading phase of the seismic safety evaluation programme.

8.2. Owing to the variety of investigations and analyses to be performed as part of the seismic safety evaluation and the need for engineering judgement by the <u>evaluation</u> team implementing the seismic safety evaluation, specific technical procedures that are specific to the project should be developed to facilitate the execution and verification of these tasks.

8.3. A peer review of the implementation of the seismic safety evaluation methodology should be performed, and documented in the management system. In particular, the peer review should assess the elements of the implementation of the SMA, SPSA or PSA-based SMA methodologies against the recommendations of this Safety Guide and current international good practices used for these evaluations.

8.4. The peer review should be conducted by experts in the areas of systems engineering, operations (including fire prevention and protection specialists); and earthquake engineering, and by other specialists depending on the focus of the seismic <u>safety</u> evaluation. Peer review should be performed at different stages in the evaluation process, as follows:

 The <u>peer</u> review of systems and operations should be performed first, coinciding with the selection of the success paths for SMA or the tailoring of the internal event system models for the SPSA or the PSA-based SMA.

2) Seismic capability peer reviews should be performed (ia) during and after the walkdown, and (iib) after a majority of the HCLPF values (for SMA or PSA-based SMA) or fragility functions (for SPSA) for the SSCs have been calculated. The seismic capability peer review should include a limited plant walkdown, which may coincide with a part of the plant walkdown or may be performed separately.

The findings of the peer reviews should be documented in the management system.

8.5. A graded approach should be used for the application of the management system to the seismic safety evaluation of nuclear installations other than nuclear power plants. The graded approach should apply to areas such as processes and activities of the seismic safety evaluation, development of technical procedures for specific tasks, and peer review of the implementation of seismic safety evaluation. In general, the application of management system requirements should be most stringent for nuclear installations with a high hazard category and least stringent for nuclear installations with a lower hazard category (see also IAEA Safety Standards Series No. GS-G-3.5, The Management System for Nuclear Installations [25]).

DOCUMENTATION AND RECORDS FOR SEISMIC SAFETY EVALUATION FOR<u>OF</u> NUCLEAR INSTALLATIONS

8.5.8.6. An important component of the management system is the definition of the documentation and records to be developed during the execution of the programme of seismic safety evaluation, and of the final report to be produced as a result of it-the evaluation. Detailed documentation should be retained for review and future applicationuse.

8.6.8.7. Typical documentation of the The results of the seismic safety evaluation should betypically be documented in a report documenting containing the following:

- (a) Methodology and assumptions of the assessment;
- (b) Selection of the reference level earthquake(s);
- (c) Composition and credentials of the evaluation team;
- (d) Verification of the geological stability <u>atof</u> the site (see para. 2.19(a));
- Success path(s) selected, justification or reasoning for the selection, HCLPF of path and controllinggoverning components of the success path(s) (for the SMA);
- (f) Summary of system models and the modifications introduced to the internal event models for the-SPSA and PSA-based SMA;



- (g) A table of selected SSC items with <u>the results of the screening process</u> (if any), failure modes, seismic demand, HCLPF values (for the SMA and PSA-based SMA) and fragility functions (for the SPSA) tabulated;
- (h) For the SPSA, results of quantification of the sequence analysis, including core damage frequency, dominant core damage sequences, large <u>or</u> early release frequency or containment failure frequency, and dominant sequences for failures of the confinement function;
- Summary of seismic failure functions for prevention and mitigation, including the frontline <u>systems</u> and support systems modelled, <u>including in SPSA</u>, and identification of critical components, if any, for the SPSA;
- (j) Walkdown report summarizing <u>any</u> findings and system wide observations, if any;
- (k) Operator actions needed and the evaluation of their likely success;
- Containment <u>structure</u> and <u>containment</u> system HCLPFs or fragility functions (if needed);
- (m) Treatment of non-seismic failures, relay chatter, dependences and <u>seismicseismically</u> induced fire and flood;
- (n) Peer review reports.

<u>8.7.8.8.</u>In addition to the above information, the following detailed information should be retained:

- (a) Detailed system descriptions used in developing the success path(s), system notebooks and other data (for SMA);
- (b) Detailed documentation of the development of the SPSA and PSA-based SMA models, in particular, those aspects pertaining to the modifications of the internal event <u>PSAprobabilistic safety assessment</u> models to account for seismic events;
- (c) Detailed documentation of all walkdowns performed, including SSC identification and characteristics, <u>results of screening process</u> (if appropriate), spatial interaction observations for the seismic system, and area walkdowns usually performed for systems such as cable trays and small bore piping, and to evaluate <u>seismicseismically</u> induced fire or flood issues;

- (d) HCLPF (for SMA and PSA-based SMA) or fragility function (for SPSA) calculation packages for all selected <u>SSC itemsSSCs</u>;
- (e) New or modified plant operating procedures for the achievement of success paths;
- (f) List of records and their retention times.

CONFIGURATION MANAGEMENT OF MODIFICATIONS FOR SEISMIC SAFETY EVALUATION FOR OF NUCLEAR INSTALLATIONS

<u>8.8.8.9.</u>The operatoroperating organization should implement a configuration programme for the management programmeof modifications to ensure that, in the future, the design and construction of modifications to SSCs, the replacement of SSCs, maintenance programmes and procedures, and operating procedures do not invalidate the results of the seismic safety evaluation.

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APPENDIX

SEISMIC FAILURE MODE CONSIDERATIONS FOR-DIFFERENT STRUCTURES, SYSTEMS AND COMPONENTS IN NUCLEAR INSTALLATIONS

A.1. The failure mode considerations identified in this appendix are typical of common classes of SSCs in nuclear installations, based on experience with previous safety evaluations. These failure modes, <u>if applicable</u>, should be reviewed and used <u>if applicable</u> to inform the <u>seismic evaluation</u> walkdown review and seismic capacity evaluations.

SEISMIC FAILURE MODES FOR BUILDINGS AND STRUCTURES IN NUCLEAR INSTALLATIONS

A.2. There are multiple potential structural failures in buildings and complex structures. Only those failure modes that might lead to accident progression to an unacceptable end state should be considered, in the seismic safety evaluation. The experience of qualified seismic capability engineers is essential in determining the potential failure modes of interest. This experience should be informed by the seismic evaluation walkdown and the review of structural drawings and previous evaluations. These The seismic failure modes for buildings and structures in nuclear installations may be broadly classified as follows:

- Local failures of structural <u>memberscomponents</u> that undermine the support of SSCs important to safety;
- (b) Major failures of structural components that lead to unacceptable deformations, misalignments, and other causes of damage or loss of function for supported SSCs;
- Major failures of structural <u>componentcomponents</u> that lead to severe damage or collapse;
- (d) Global structure instability (e.g. sliding, overturning, and foundation bearing failure).
- (e) Failures of structures that are part of containment or confinement systems, which <u>canmight</u> lead to a radioactive release-.

A.3. Relative movements between adjacent structures should be considered with respect to the existing separations and whether <u>theythe structures</u> are constructed on common or separate foundations. The associated potential failure modes may be classified as follows:

- (a) Major failure of one structure due to impact withby a significantly heavier structure;
- (b) Local failures in the structure exteriors due to impact (e.g. punching of walls);
- (c) Failures of chatter-sensitive electrical components due to impact between structures;
- (d) Failures of other shock-sensitive SSCs or SSC supports in the vicinity of impact;
- (e) Failures of distribution systems or their supports due to separationsrelative movements between <u>adjacent</u> structures.

A.4. <u>Seismic The seismic</u> capacity evaluation of structures should be based on available construction information. The review of the structures during the walkdown should focus on supplementing this information with as-built observations. <u>Example data to focus on include, including in relation to</u> the following:

- (a) Potential signs of degradation or distress, such as corrosion, exposure of reinforcement, and concrete spalling;
- (b) Records of structure connections that appear to be field-modified from standard connections;
- Measurements of interface separations between buildings, and description of gap filler materials, if present;
- (d) Survey of equipment that enables the estimation of temporary loading during maintenance or refuelling conditions⁶⁰;
- (e) Survey of as-built versus as-designed <u>bulk storage spaces (mass capacity)</u>, roof equipment, storage, and roofing materials.

SEISMIC FAILURE MODES FOR MECHANICAL EQUIPMENT IN NUCLEAR INSTALLATIONS

A.5. Mechanical equipment in nuclear installations typically includes process equipment, pumps, tanks and heat exchangers, fans and air handlers, and valves. The review of theirthe seismic capacity of these items should include the quality of their anchorage, support structure, mounting configuration, equipment construction, and the ability of the equipment to function. Some damage to the equipment is tolerable if it does not compromise itsthe equipment's ability

⁶⁰ While equipment masses may be estimated from the structure design drawings for individual floors, some areas may be designed for heavy loads that are only experienced infrequently, typically when the installation is not in operation. A typical example of this is a laydown area where a nuclear reactor head is temporarily stored during a refuelling outage.

to perform its credited function-(e.g. active function) or its leaktightness or structural integrity. The functional assessment includes-should include time considerations (e.g. such as whether thea component is needed to operate during or after the earthquake shaking, and the duration of that operation for how long without outside support). It. The assessment should also include an assessment of potential seismic interactions and the flexibility of attached distribution system lines.

A.6. <u>The For the</u> review of mechanical equipment with considerable oil content<u>should</u> consider, potential failure modes that <u>canmight</u> result in oil leakage and subsequent fire (e.g. breakage of oil level sight glass monitors on pumps), should be considered.

A.7. Mechanical equipment with substantial piping (e.g. tanks, heat exchangers, and pumps) should also be reviewed for potential nozzle loads from the inertia of the attached piping.

A.8. The For the review of mechanical equipment supported on vibration isolators should consider their, the potential failure due of the isolators owing to shaking-induced displacement should be considered.

A.9. The mountings of valves and pump shafts <u>supported</u> independently-<u>supported</u> from the attached piping and pumps, respectively, should be reviewed for potential differential motion failures.

SEISMIC FAILURE MODES FOR ELECTRICAL EQUIPMENT IN NUCLEAR INSTALLATIONS

A.10. Electrical equipment includes instrumentation and control panels, switchgearswitchgears, transformers, inverters, generators, and batteries. The review of theirthe seismic capacity of electrical equipment should include the same considerations as for mechanical equipment, identified in paras. A.5 and A.6. Many types of electrical equipment are typically vulnerable to spray (e.g. from overhead fire protection sprinklers).

A.11. The review of electrical cabinets should <u>considerinclude checking</u> whether the internal instruments and components are positively and securely attached inside the enclosure and whether their mountings are stiff or flexible. In <u>particular, if If</u> the internal instruments and components are on a structure that can be pulled out <u>fromof</u> the cabinet <u>from the viewpoint</u> <u>offor</u> maintenance, the amplification of seismic motion due to this structure should be <u>consideredgiven particular attention</u>.

A.12. The review of electrical cabinets that contain chatter-sensitive components should

considerinclude checking whether the cabinets are adequately spaced and/or whether they have adequate spacing or are bolted to the adjacent cabinets to prevent pounding.

A.13. The review of diesel generators should include the exhaust and ventilation systems.

A.14. The review of batteries should <u>considerinclude checking</u> whether they are adequately spaced and restrained. <u>Inadequately spaced and restrained batteries might be damaged</u> themselves by shaking, and might damage other nearby components through the spillage of <u>acid</u>.

SEISMIC FAILURE MODES FOR INDIVIDUAL INSTRUMENTS AND DEVICES IN NUCLEAR INSTALLATIONS

A.15. Local instruments and passive elements in nuclear installations are usually seismically rugged SSCs. TheFor the review of their seismic capacity should consider, the adequacy of the mounting, the flexibility of the attached lines, and potential spatial interactions. It should also consider thebe considered. The consequences of failure on the SSC function of interest (e.g. potential breakage of the glass cover on the reporting dial of a sensor). should also be considered.

A.16. Chatter-sensitive devices may include electromagnetic relays, switchgear circuit breakers, motor starters, and indicator switches for temperature, pressure, level, or flow. The review of theirthe seismic capacity of chatter-sensitive devices should considerinclude the seismic qualification of the device model, the height and theirmeans of attachment to the equipment component that hosts them the device, and any spatial interaction concerns that might affect the host component or the device directly. These Chatter-sensitive devices are typically very sensitive to transmitted shock waves resulting from impact or pounding. Chatter The chatter of these devices may be recoverable through operator actions. If credit is taken for If these operator actions are credited, an evaluation of the reliability of these the actions after the earthquake, the time available to successfully implement these the actions and the associated travel paths should be included in the analysis review.

SEISMIC FAILURE MODES FOR DISTRIBUTION SYSTEMS IN NUCLEAR INSTALLATIONS

A.17. Distribution systems include piping, sampling points, cable trays and conduits, and ducting. These systems have typically high seismic capacities due to their relatively light weight and substantial ductility, since yielding in itself does not prevent the performance of their safety

function. The seismic capacity review of <u>thesedistribution</u> systems should be performed on an area basis (e.g. in a room or corridor) and <u>considerinclude</u> representative configurations identified to be potentially vulnerable during the seismic <u>evaluation</u> walkdown (see para. 5.31). Seismically vulnerable conditions include the following:

- (a) Differential motion between supports or attachment points;
- (b) Flexible supports and other details that <u>canmight</u> allow large seismic displacements;
- (c) Weak or brittle connections, supports, or anchorage;
- (d) Long flexible runs connected to stiff branch lines or supports;
- (e) Excessively loaded supports (e.g. multiple or overfilled cable trays or long spans);
- (f) Degradation and corrosion.

SEISMIC INTERACTION CONSIDERATIONS FOR FAILURE OF SSCs IN NUCLEAR INSTALLATIONS

A.18. Common sources of spatial interaction include pounding between adjacent SSCs or their support structures, masonry walls, unsecured light fixtures, unanchored objects, overhead cranes, suspended ceilings, and temporary structures left in place (e.g. scaffolding).) left in place. The seismic capacity review of potential spatial interaction sources should consider both the credibility and the consequences of the interaction. For example, a falling hazard from an unsecured lightweight overhead light fixture will have no consequence on an electrical cabinet that contains no soft targets or chatter-sensitive devices and, so need not be explicitly evaluated.

A.19. The For the review of seismic-_fire interactions-should consider, the ignition sources previously identified in the internal fire safety assessment--should be considered. Only ignition sources that can<u>might</u> be potentially-initiated by seismic-seismically induced failure modes should be considered. This review should also include: (ig) potential failure modes of items on the list of selected SSCs list-that can<u>might</u> lead to fire-ignition of a fire that spreads to adjacent SSCs_{x2} and (iib) additional SSCs identified during the area-_based seismic evaluation walkdowns as potential ignition_sources (e.g. non-safety-_related high-_voltage electrical cabinets or transformers) in applicable proximity to any of the selected SSCs. The fire area affected by each potential ignition source should be determined by the systems engineer considering, taking into consideration the presence of combustibles, fire protection_x and possible spread dueowing to the failure of boundaries.

A.20. The<u>For the</u> review of seismic-flood interactions-should consider, the flood sources

previously identified in the internal flood safety assessment, <u>should be considered</u>. Only the flood sources that <u>canmight</u> be <u>potentially</u>-initiated by <u>seismic-seismically</u> induced failure modes should be considered. This review should also include: (ia) potential failure modes of items on the <u>list of</u> selected SSCs <u>list</u> that <u>canmight</u> lead to a flood that spreads to adjacent SSCs_{ri} and (iib) additional SSCs identified during the area-_based seismic <u>evaluation</u> walkdowns as potential flood_sources (e.g. unanchored tanks, non-ductile piping, <u>and</u>-non-safety-_related heat exchangers) that <u>canmight</u> affect any of the selected SSCs. The flood area affected by each potential source should be determined by the systems engineer-<u>considering</u>, <u>taking into consideration</u> the volume of released fluid, flow paths within a floor plan and from higher to lower elevations within a building, potential barriers or path diversions inside the building, and the configurations of the SSCs in the flooded area(s).

A.21. The<u>For the</u> review of seismic-__flood and seismic-__spray interactions-<u>should consider</u>, the seismic vulnerabilities of the fire protection systems, <u>overhead rainwater drainage lines</u> and other non-ductile piping<u>- should be considered</u>. Experience has shown that these<u>fire protection</u> systems are susceptible to <u>seismic-seismically</u> induced shaking. Known vulnerabilities of fire protection systems include mechanical couplings, threaded pipe connections, easy-to-damage sprinkler heads (i.e. <u>due-todamage by</u> impact with adjacent objects) in wet systems, and inadvertent actuation of dry systems. <u>SeismicThe seismic</u> capacity review of <u>thesefire protection</u> systems should be performed on an area basis, as described <u>for distribution systems</u> in para. A.17, <u>considering</u>-in particular <u>taking into consideration</u> the proximity of known seismically deficient system components to spray-sensitive SSCs.

OPERATOR TRAVEL PATHS

A.22. TheIn order to review seismic capacities that should be reviewed depend on the understanding of the expected movements necessary to execute operator actions credited in the seismic safety evaluation should be understood, and on considering seismic seismically induced failures that maymight impede access to, travel along, or egress along from these paths-should be taken into consideration. Common potential impediments to travel include masonry walls that maymight collapse and block a pathway, normally shut doors that maymight be distorted dueowing to seismic damage and rendered unopenable, seismic-seismically induced fire and flood along the travel path, and blocked access to tool storage locations of tools.

A.23. If outside help is credited in the safety evaluation, the seismic capacity review should also consider potential failures along additional travel paths that are needed for the arrival and

deployment of this help within the necessary time. Examples include critical highway bridges and, road juncturesjunctions, access roads to the nuclear installation, and entry points to the buildings.

SPECIFIC CONSIDERATIONS FOR SEISMIC FAILURE MODES FOR NUCLEAR POWER PLANTS

A.24. An explicit evaluation of the seismic capacity of the primary reactor system and components should be performed. A review of design documentation and previous evaluations should be performed to identify credible <u>seismic seismically</u> induced failure modes. The candidate failure modes should be evaluated using the seismic demands of the reference level earthquake to identify the governing failure mode or modes. Several governing failure modes may be identified that lead to different consequences for the installation end state.

A.25. The seismic capacity of the primary (and secondary, if applicable) containment should be explicitly evaluated. All credible <u>seismic_seismically</u> induced failure modes that <u>canmight</u> lead to <u>a</u> loss of structural integrity in the containment pressure boundary should be included.

NON-VIBRATORY GROUND MOTION-_INDUCED FAILURES IN NUCLEAR INSTALLATIONS

A.26. Potential SSC failure modes due to geotechnical failure hazards that could not be screened out (see paras- 2.19 and 5.11) should be considered in the seismic <u>evaluation</u> walkdown and <u>seismic</u> capacity review. The corresponding seismic demands are typically permanent displacements rather than accelerations. The seismic capacity review of the affected SSCs should focus on <u>their abilitythe capacity of the SSCs</u> to perform their credited functions when subjected to the imposed displacements. This capacity will typically depend on the flexibility and ductility of <u>the</u> attached distribution systems, which should, if feasible, be assessed during seismic <u>evaluation</u> walkdowns, as follows. Particular attention should be paid to the following conditions that might affect the distribution systems:

- (a) Settlement of structure foundations due to liquefaction, groundwater drawdown or dry sand settlement maycompaction, which might result in the failure of buried distribution systems at thetheir interface with the structure;
- (b) Relative vertical displacements between adjacent structures due to differential settlement<u>may</u>, which might result in the failure of interconnecting distribution systems;

- (c) Differential settlements under the foundations of a structure-<u>may, which might</u> result in <u>the</u> permanent distortion, <u>of</u>, <u>or</u> internal damage to <u>structure members</u>, <u>structural</u> <u>components</u> and/<u>or</u> failures of attached lines;
- (d) Slope displacements mayand potential instabilities, which might result in the failure of buried and abovegroundabove ground lines and of SSCs below the slope;
- (e) Fault rupture, subsidence, and lateral spreading displacements <u>may, which might</u> result in <u>the failure of buried and abovegroundabove ground</u> lines and <u>of</u> SSCs spanning the ground displacement zone.

A.27. Potential SSC failure modes due to concomitant phenomena that could not be screened out (see paras 2.19 and 5.11) should be considered in the seismic <u>evaluation</u> walkdown and <u>seismic</u> capacity review, for example, as follows:

- (a) The seismic capacity of an upstream dam whose breach <u>cannight</u> result in flooding of the nuclear installation site should be explicitly evaluated. This seismic capacity should be mapped to the consequences on the installation in accordance with SSG-18 [1413], considering the vulnerability of individual SSCs to the flood level and the lower reliability of emergency response procedures in the combined aftermath of earthquake and flood.
- (b) The assessment of the consequenceconsequences of a tsunami hazard on the safety functions of <u>a</u>_nuclear installationsinstallation located near coastlines the coastline should include evaluating the potential malfunctioning of equipment located at a low level, such as (e.g. seawater pumps), in accordance with SSG-18 [1413] and IAEA Safety Standards Series No. NS-G 1.5, SSG-68, Design of Nuclear Installations Against External Events Excluding Earthquakes in the Design of Nuclear Power Plants [24];[26].
- (c) The seismic slope stability and displacement capacity of geographic features close to the nuclear installation site (e.g. slopes that might trigger a landslide, a rockfall event that could might affect the nuclear installation site) should be explicitly evaluated. The consequences of this landslidethese geographic features on the installation's safety-related functions should be assessed, considering the slope-discharge along the landslidefailure path and the distance to the installation.

(d) The potential for seismic failures in adjacent nuclear and industrial facilities installations that might affect the nuclear installation in question should be identified during the walkdown and reported for further assessment.

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ANNEX

EXAMPLE OF CRITERIA FOR DEFINING SEISMIC DESIGN CLASSESCATEGORIES AND PERFORMANCE TARGETS IN NUCLEAR INSTALLATIONS

SEISMIC DESIGN CLASSESCATEGORIES FOR SSCs IN NUCLEAR INSTALLATIONS

A–1. Table A–1 provides an example of criteria for defining seismic design classescategories⁶¹ of SSCs in a nuclear installation, taken from the practice of one Member State (United States of America) [A–1]. SSCs with a safety function are assigned into one of the five <u>seismic design</u> classes given in the table, based on the unmitigated consequences that <u>maymight</u> result from the failure of the SSC by itself or in combination with other SSCs.

A–2. A similar approach has been used to categorize nuclear installations into high (SDC-seismic design classes 4, SDC- and 5), moderate (SDCseismic design class-3) and low (SDC-seismic design classes 1, SDC- and 2) hazard categories, in accordance with the risk to the public, workers, or the environment from a potential unmitigated radioactive release [A–1]. These hazard categories are also shown in Table A–1.

PERFORMANCE TARGETS FOR SSCs AND NUCLEAR INSTALLATIONS FOR SEISMIC EVALUATION PURPOSES

A–3. A <u>performance target_target</u> is a selected annual frequency of failure due to the earthquake hazard. Performance targets are linked to seismic design <u>classescategories</u> for SSCs. Table A–2 shows an example of selected performance targets taken from the practice of one Member State (United States of America) [A–2].

A-4. In Table A-2, the <u>performance targets range from the</u> annual frequency of failure (performance target) ranges from that assumed for normal building structures in some Member States (i.e. about $P_f = 10^{-3}$ per year) to <u>thata frequency</u> approaching <u>athe</u> mean core damage frequency for seismically induced core melt, <u>which that</u> is considered acceptable in some Member States (i.e. about $P_f = 10^{-5}$ per year). The performance targets for the intermediate

⁶¹ Seismic design categories are referred to as 'seismic design classes' in Table A-1 and Table A-2. 100

seismic design <u>classescategories</u> are between these two values.

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TABLE A–1. SEISMIC DESIGN CLASS BASED ON THE UNMITIGATED CONSEQUENCES OF FAILURE [A-1] (COURTESY OF THE AMERICAN NUCLEAR SOCIETY)

Seismic Design Class	Hazard Category	Unmitigated Consequences of Failure		
		Worker	Public	Environment
1ª		No radiological or toxicological release consequences but failure of SSCs may place facility workforce at risk of physical injury.	No radiological or toxicological release consequences.	No radiological or toxicological release consequences.
2ª	Low	Radiological/toxicological exposures to workers will have no permanent health effects, may place more facility workers at risk of physical injury, or may place emergency operations at risk.	Radiological/toxicological exposures of public areas are small enough to require no public warnings concerning health effects.	No radiological or chemical environmental consequences.
3	Moderate	Radiological/toxicological exposures that may place facility worker'sworkers' long-term health ⁶² in question.	Radiological/toxicological exposures of public areas would not be expected to cause health consequences but may require emergency plans to assure protections.	No long-term environmental consequences are expected, but environmental monitoring may be required for a period of time.
4	High	Radiological/toxicological exposures that may cause long-term health problems and possible loss of life for a worker in proximity of the sources of hazardous material, or place workers in nearby on-site facilities at risk.	Radiological/toxicological exposures that may cause long-term health problems to an individual at the exclusion area boundary for two hours.	Environmental monitoring required and potential temporary exclusion from selected areas for contamination removal.
5		Radiological/toxicological exposures that may cause loss of life of workers in the facility	Radiological/toxicological exposures that may possibly cause loss of life to an individual at the exclusion area boundary for an exposure of two hours.	Environmental monitoring required and potentially permanent exclusion from selected areas of contamination.

Notes:

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⁶² The term 'long-term health problems' in the context of radiation exposure corresponds to the term 'stochastic effects' in the IAEA's terminology (see Ref. [A-2]).

(a) <u>"</u>No radiological<u>for</u> toxicological <u>releases</u>" or <u>"releases</u>' and 'no radiological<u>for</u> toxicological <u>consequences</u>" <u>meansconsequences</u>' <u>mean</u> that material releases that cause health or environment concerns are not expected to occur from failures of SSCs assigned to seismic design classes 1 or 2.

Seismic Design Class	Hazard Category	Performance target (yr ⁻¹)
1	Low	< 1 × 10 ⁻³
2		<4×10 ⁴
3	Moderate	~ 1 × 10 ⁴
4	High	~ 4 × 10 ⁻⁵
5		~ 1 × 10 ⁻⁵

TABLE A–2. EXAMPLE OF PERFORMANCE TARGETS [4A-2] (COURTESY OF THE AMERICAN SOCIETY OF CIVIL ENGINEERS)

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REFERENCES TO ANNEX

- [A–1] AMERICAN NUCLEAR SOCIETY, «Categorization of Nuclear Facility Structures, Systems, and Components for Seismic Design, » <u>Standard ANSI/ANS 2.26-2004 (R2010, R2017), ANS</u>, La Grange Park, <u>Illinois, IL (2017-).</u>
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